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CoA Memo No. 98

April, 1966

THE COLLEGE OF AERONAUTICS
DEPARTMENT OF PRODUCTION AND INDUSTRIAL ADMINISTRATION
MACHINE TOOLS LABORATORY



A report on a series of tests carried out to determine
the suitability of the grinding process for evaluating
the efficiency of coolants to be used on the metal
cutting processes and also to evaluate the relative
efficiency of 4 coolant samples for the drilling
and turning processes

- by -

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Introduction

A test programme was to be carried out to evaluate a series of additives for use in industrial metal cutting coolants for use initially on the turning, drilling and milling processes. These tests when they take the form of tool life tests are costly in time and material and where a shorter test can be reliably substituted for a life test, this is most desirable. To this end the grinding process was included in a pilot scheme to try to relate the grinding results to the drilling and turning results. Milling was not used in this pilot scheme.

The grinding process has been very extensively studied at the College of Aeronautics during the past 10 years and a reliable method of evaluating the performance of grinding wheels and coolants has been developed and proved in a very wide range of industrial applications. The time required to evaluate a wheel or coolant sample is approximately 1 hour and the material consumed would be a few ounces in weight, hence, the desire to interpret coolant efficiency for the metal cutting processes from tests carried out using the controlled grinding process. (See ref. 1).

Summary

The coolant samples were not identified by their chemical composition, but by numbers from 1 to 4. Each was evaluated for efficiency when used on the grinding process. The results of these tests show the following order of efficiency.

Coolant sample No. 4 was most efficient, with sample No. 3 next best.
Coolant sample No. 2 was more efficient than No. 1.
Coolant sample No. 1 was least efficient.

The summary and results sheets are included at the end of this report.

The coolant samples were then tested on the turning process. Tool life to a flank wear land of 0.017 to 0.020 ins. was taken as the end of a tool life. The tests were carried out under close control and observation and all tools were used once only and preserved after test to afford comparison one with another.

The results are recorded and included at the end of this report and summarised on Results Sheet Fig. 6 from which it is shown that Coolant Samples Nos. 1, 2 and 3 are in the same order of efficiency as for the grinding process. The characteristics of the slope of the curves would appear to confirm the grinding results in that they became more efficient as the surface speed in turning increases, or temperature plays a more critical role. The relative efficiency of the Samples Nos. 1, 2 and 3 change order at speeds below about 40 ft. per minute.

No. 1 would be most efficient. No. 2 next best, and No. 3 would be least efficient.

These results should be reflected in the drilling process results. They should show that failure is more evident on the radial points when coolant sample No. 3 is used, and that point wear radial cutting edge wear and chisel point failure all play a part when coolant No. 2 is used. With Coolant No. 1 showing a more even wear than either No. 3 or No. 2, and this is evident to some extent from the details of drilling test results, which are included at the end of this report. Though the limited time available proved inadequate to produce sufficient drilling results to be reliable for the evaluation on which a development programme for coolant additives can be based, this is not so on the grinding and turning processes. These are completely reliable. Coolant No. 4 is consistently producing performance results which are at variance to the other samples, and from these results it is assumed that this coolant has a different chemical analysis to the others. No. 4 coolant is most efficient when used on the grinding process, and least efficient on the turning and drilling processes, however, it performs with some correlation between the turning and drilling processes in a similar manner to the other samples in that on turning at higher surface speeds it is less efficient than at the lower speeds and the drilling results for Sample No. 4 show that radial corner failure occurs in more prominence than chisel point failure, i.e. the low speed high pressure conditions are coupled with more efficiency.

Conclusions

The results recorded from the limited amount of work carried out during approximately 30 working days, by two development engineers is inadequate to form a rigid conclusion. The results show that the grinding process and turning process can be related for chemically similar products where only the amounts of each element is varied. There would appear to be some confusion when the chemical content is varied, though the results obtained when chemical composition is varied stand logical analysis. This also applies to the results which from the tests carried out show more confusion than turning and grinding, and a valid conclusion to be drawn from the drilling results would be that more time is needed and a wider range of data must be recorded to substantiate the correlation. Work should be carried out on the milling process. The results obtained in all processes used stand up to logical analysis.



The Test Work

The material

All the test material was purchased at one time from Herringshaw Steels Ltd. of Birmingham. It was taken from one melt. A certificate of analysis was obtained from the suppliers. The details are as follows:

Material 6 inch diameter forged bar in the annealed condition.
To specification EN 24.

Cast LF 1063

Analysis

C	Si	Mn	S	P	Ni	Cr	Mo
0.41	0.28	0.62	0.029	0.013	1.47	1.14	0.26

Signed: R.J. Cantingell dated 5th August, 1965.

Our Order No. 7676.

Photographs of the material structure are included in M1 and M2.

The material was sawn into lengths 2 ft. 9 ins. long. These were used for the turning tests. A 10 inch length was used for the grinding tests. A flat was shaped down the axial length to provide a stable base for mounting on the magnetic chuck. Two 2 ft. 9 in. lengths were sawn into 1 inch thick slices to provide the drilling test pieces. These drilling slices were faced up on the lathe, one of them was also surface ground, and a hardness plot made across the section. The results of this plot are shown in Fig. 1.

The Coolants

Four samples of coolant were supplied by ICI of Runcorn, Cheshire. Approximately 20 gallons of each sample being provided. The identity of the coolants were not revealed. This arrangement avoided any tendency towards bias results, hence on the result sheets reference is made to Coolants Nos. 1, 2, 3 and 4.

Every precaution was taken to avoid any contamination of one coolant sample with another. All containers were wiped clean between tests and a small volume pumped through the system and discarded every time the coolant sample was changed.

Analysis of results from the grinding tests

All conditions other than the coolants remained constant. Full details of the test conditions and grinding wheel specification are recorded on the result sheets which are reproduced at the end of this report. The test method is based on that developed at The College of Aeronautics¹. The significant figure when evaluating coolant efficiency is the surface area ground between each grit row breakdown on the alpha angle. This is because the coolant influences grit wear by way of reducing the coefficient of friction between the chip and the grit. An efficient coolant will reduce the friction and hence grit wear is reduced and a less efficient coolant will allow the friction to reach higher values, resulting in a more rapid rate of wear on the grits.

It is necessary to eliminate any variables in the test runs as far as is practical and to this end the first result in each test are discarded. This has been done because when the wheel is set in cross traverse, it may contact the work differently on the first impact. As this procedure is repeated on all tests analysis the correctness of this is not challenged.

The surface area ground between each grit row failure other than the first are arithmetically averaged. These averages are assumed to reflect the efficiency of the coolants.

The most efficient coolant will cause the grits to perform the greatest amount of work between grit row failure and the least efficient will result in grit failure occurring more frequently. This is due to the rate of grit wear being higher.

A summary of the results showing the area ground between each grit row failure from which it is seen the relative efficiency of each coolant is included SG.1.

Note the initial corner breakdown and the area ground between this and the first grit row failure is not summarised. The results are recorded on the result sheets G.1 to G.10. * indicates the start of the valid results for coolant evaluation tests.

The tests on the turning process

These tests were carried out on a Colchester Lathe 8 inch centres, in new condition. The lathe tools were $\frac{3}{4}$ inch diameter and taken from the same bar stock as that from which the drills were made, each tool piece was subjected to a hardness test. The Vickers pyramid method was used and the results of these tests are recorded on Test Sheet T.H.1, from which it will be seen that they were very similar in hardness ranging from VPN 840 to VPN 870.

The tools were ground on a surface grinding machine using a tool

grinding jig and ample supply of coolant. The cutting angles were produced on both ends of the 3 inch long tool pieces as follows:

The ground faces were re-checked for hardness after grinding.

British Standard Terms and Definitions for Single Point Cutting Tools² 1886 1952.

Cutting Edge Side Rake	15°
Plan Approach Angle	5°
Plan Trail Angle	6°
Cutting Edge Back Rake	0°
Front and Side Clearance Angle	6°
Nose Radius	.040 ins.

All tools were hand lapped and examined for quality of the cutting edges under a 25 to 1 microscope.

The tools were used once only. The 48 cutting edges providing 9 for each of the 4 coolant samples and 12 for repeat runs and spot check runs. In this way the worn tools were preserved and can be compared one with another. Typical worn tools are shown in Figs. 2, 3, 4 which shows a cratered tool a chipped cutting edge and flank wear. The Taylor Hobson Talisurf was used to measure top face cratering. A typical trace is shown in Fig. 5. The cutting conditions were as follows:

The tools were located rigidly in a jig which was carried in the lathe tool post.

Feed per revolution remained constant at 0.005 ins. rev.

Depth of cut remained constant at 0.100 inches.

Surface speed was the VARIABLE. This was achieved using the infinitely variable speed 25 h.p. motor which is fitted to the lathe and a tachometer. The speed was checked frequently under cutting conditions.

The results of the turning tests were plotted as $VT^n = C$ curves³, and are reproduced in Fig. 6. The same results are presented on normal bases in Fig. 7, and the tabulated measurements from which the curves are plotted are included in the test result sheets. TURNING TESTS at the end of this report.

From these test results it is seen that Coolant Sample No. 3 is most efficient. Coolant Sample No. 2 is a close second, and Sample No. 1 is least efficient. Coolant No. 4 is between No. 1 and 2.

This later sample No. 4 is to a different specification from the other samples.

The Drilling Tests

Tests carried out to evaluate the coolants efficiency for the drilling process were carried out on a 4 ft. 6 in. radial arm drilling machine. The workpieces were carried in an indexing 3 jaw chuck. This could be indexed to allow speedy radial spacing of the drilled holes and the movement of the radial arm afforded adjustment for the consecutive rings of holes. In this way the whole of the surface of the test piece could be drilled with the very minimum of waste material and manipulation time.

The radial arm drilling machine is equipped with an integral coolant well contained within the base of the machine casting and no attempt was made to use this due to the difficulty of assuring non-contamination of the coolant samples and a second coolant system which is that fitted to a $\frac{3}{8}$ " capacity multi-spindle drilling machine stood next to the radial arm machine.

To achieve the full benefit from this external coolant system with its small square tank the work holding indexing chuck was mounted on the radial arm machine table, stood in a shallow tank (the bottom half of a 10 gallon oil drum), holes being made in the bottom through which the table bolts could pass. Rubber sheet was used to seal the tank on the table, a further outlet hole was arranged to return the coolant from this tank via a $\frac{1}{2}$ in. diameter plastic tube to the supply tank, a further $\frac{1}{2}$ inch tube was fitted over the multi-spindle coolant outlet and arranged to supply the test drill. There was some loss in pressure, but the supply was more than needed.

The time which was available for these tests proved too short to maintain the full range of data records which were described in a previous report on this test work, and after a short time it was realised that the tool wear data must become the only data collected. This was because it may be assumed that the wear criteria is most important, and duplication would consume more time than was available.

The drilling process is more difficult to evaluate than many other processes. This is recognised to be due to the geometry of the drill cutting edges which is infinitely variable between the extreme of the chisel point and the radial corners, and when to this variable geometry the variable cutting speed which is from zero at the drill centre to maximum at the radial corner and the very severe interference from the swarf is taken into account. The results of any test programme will reflect the extent of control and volume of data collected. This is evident in the results included in this report on Drilling test sheets and summarised on SD1. The details of the drill point geometry and drilling conditions are included on the test result sheets. Figures 8, 9 and 10 shows the variety of wear suffered by the drill points and further emphasises the necessity to record all data to enable a comparative conclusion to be made.



References

1. The College of Aeronautics Report on The numerical analysis of the grinding process.
2. British Standard Specification on Single Point Cutting Tools. 1886 1952.
3. The Art of Metal Cutting by Taylor. VTⁿ-C.

VPN HARDNESS TRACE ON CROSS SECTION OF 6 INCH
DIAMETER BAR OF THE TEST MATERIAL (EN 24 IN THE
ANNEALED CONDITION 20 Kg LOAD.)

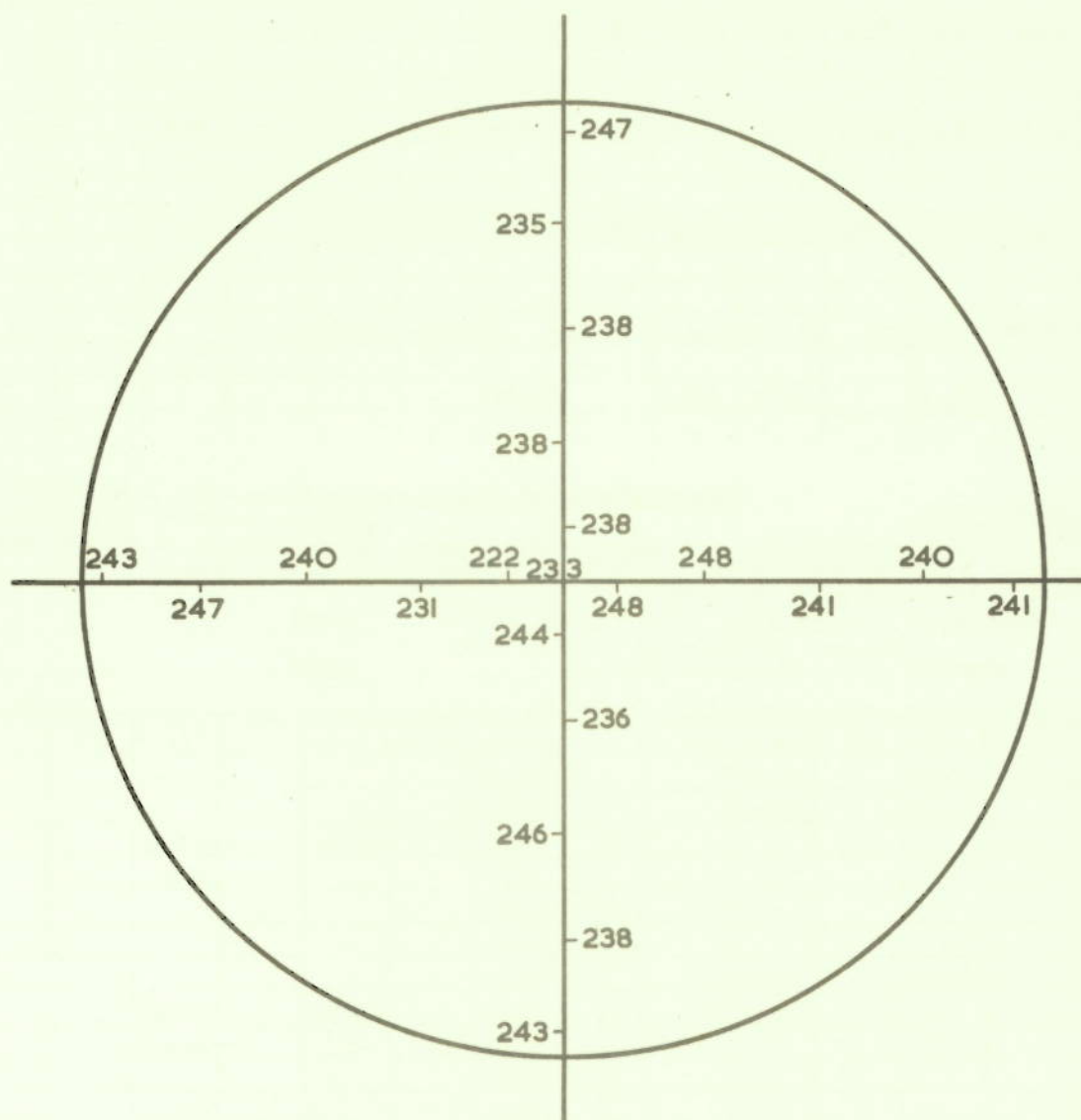


FIG. I.

60 grit wheel.

The College of Aeronautics

EXPERIMENTAL RECORD GRINDING TESTS

SG 1

EXPERIMENT: COOLANT EVALUATION TESTS

NAME

REMARKS: SUMMARY OF GRIT ROW & WEAR.

DATE

	SURFACE AREA GROUND BETWEEN EACH GRIT ROW FAILURE SQ.INS.										
COOLANT SAMPLE											AVERAGE
No 1	140	100	140	120	100	60	140	140	140	100	118
No 2	140	120	160	140	160	160	120	120	180		144
No 3	160	160	200	180	140	240	120	140			167
No 4	200	220	240	200	240	200	200	220	180		211
THE ORDER OF INCREASING EFFICIENCY IS.											
	No 1	No 2	No 3	No 4							

CONDITIONS

DEPTH OF CUT = 0.001 INS

TABLE SPEED = 65 FT/MIN

CROSS FEED = 0.042 INS/STROKE

The College of Aeronautics

COOLANT SAMPLE No 1

GRINDING WHEEL SPEC. UNI-MA-60-HV

WORK PIECE EN 24 ANNEALED

VPN 246

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME

G 1

REMARKS: RESULTS B = 0.100 INS L = 0.054 INS
E = 0.00042 INS

DATE

SURFACE AREA GROUND SQ.INS	WHEEL FACE WIDTH INS	WHEEL FACE LOST INS	SURFACE AREA GROUND SQ.INS	WHEEL FACE WIDTH INS	WHEEL FACE LOST INS
START OF TEST	0.720	NONE	460	"	NONE
40	0.620	0.100	480	"	"
60	"	"	500	0.570	0.090
80	"	"	520	"	NONE
100	"	"	540	"	"
120	"	"	560	"	"
140	0.600	0.020	580	"	"
160	"	NONE *	600	0.490	0.020
180	"	"	620	"	NONE
200	"	"	640	"	"
220	"	"	680	"	"
240	0.570	0.030	700	"	"
260	"	NONE	720	"	"
280	"	"	740	0.450	0.052
300	"	"	760	"	NONE
320	"	"	780	"	"
340	"	"	800	"	"
360	0.550	0.020			"
380	"	NONE	END OF TEST		
400	"	"			
420	"	"			
440	"	"			

CONDITIONS

DEPTH OF CUT = 0.001 INS.
TABLE SPEED = 65 FT/MIN.
CROSS FEED = 0.042 INS/STROKE.

The College of Aeronautics

COOLANT SAMPLE No 2.

GRINDING WHEEL SPEC UNI-MA-60-HV.
WORKPIECE EN 24 ANNEALED
VPN 240.

EXPERIMENTAL RECORD GRINDING TESTS

EXPERIMENT: COOLANT EFFICIENCY TESTS

RESULTS B = 0.100 INS L = 0.054 INS

REMARKS: E = 0.00042 INS A = 0.1 TO 0.13 CUB. INS

NAME: J. PURCELL - T. CHATER

DATE

93

SURFACE AREA GROUND SQ. INS.	WHEEL FACE WIDTH	WHEEL WIDTH LOST	SURFACE AREA GROUND	WHEEL WIDTH	WHEEL WIDTH LOST	AREA GROUND	WHEEL FACE WIDTH	WHEEL WIDTH LOST
START No 1	0.720	NONE	START No 2	0.730	NONE	320	0.570	NONE
40	0.620	0.100	20	0.630	0.100	340	"	"
60	"	NONE	40	"	NONE	360	0.500	0.070
80	"	"	60	"	"	380	"	NONE
100	"	"	80	END OF TEST.		400	"	"
120	"	"				420	"	"
140	"	"	START No 3	0.730	NONE	440	"	"
160	"	"	20	0.630	0.100	460	"	"
180	0.570	0.050	40	"	NONE	480	"	"
200	"	NONE *	60	"	"	500	"	
220	"	"	80	"	"	520	0.460	0.040
240	"	"	100	"	"	540	"	NONE
260	"	"	120	"	"	END OF TEST		
280	"	"	140	"	"			
300	"	"	160	"	"			
320	"	"	180	"	"			
340	0.510	0.060	200	0.570	0.060			
360	"	NONE	220	"	NONE *			
380	"	"	240	"	"			
400	"	"	260	"	"			
420	"	"	280	"	"			
440	END OF TEST		300	"	"			

CONDITIONS

The College of Aeronautics

DEPTH OF CUT = 0.001 INS

THICK SPEED = 65 FT/MIN.

CROSS FEED = 0.042 INS/STROKE

EXPERIMENTAL RECORD

COOLANT SAMPLE No 2
GRINDING WHEEL SPEC UNHMA, 60. HV
WORK PIECE EN 24 ANNEALED
VPN 246

EXPERIMENT: COOLANT EFFICIENCY TEST

NAME _____

RESULTS $B = 0.000$ $L = 0.054$

REMARKS: $E = 0.00042$

DATE _____

95

SURFACE AREA GROUND SPINS	WHEEL FACE WIDTH INS	WHEEL FACE LOSS INS	SURFACE AREA GROUND SPINS	WHEEL FACE WIDTH INS	WHEEL FACE LOSS INS
17.5	.680	.040	START	.730	NONE
35.0	.620	.060	17.5	.630	0.100
52.5	"	NONE	35	"	NONE
70.0	"	"	52	"	" NOT SUMMARISED
87.5	"	"	70	"	"
105.0	"	"	87	"	"
122.5	"	"			
140.0	"	"	START	.730	NONE
157.5	"	"	17	.620	0.100
175.0	"	"	35	"	"
192.5	.510	.110	52	"	"
210.0	"	NONE *	70	"	"
227.5	"	"			
245.0	"	"	START	.720	NONE
252.5	"	"	17	.620	0.100
270	"	"	35	"	NONE
287	"	"	52	"	"
305	"	"	70	"	"
322	"	"			
340	.450	.060			

THESE TESTS WERE CARRIED OUT TO
CHECK THE PROPORTIONS OF ALPHA.
AND E, L, B.

CONDITIONS

DEPTH OF CUT = 0.001 INS
TABLE SPEED = 65 FT/MIN
CROSS FEED = 0.042 INS/STROKE

The College of Aeronautics

EXPERIMENTAL RECORD

GRINDING TESTS

COOLANT SAMPLE No. 3

GRINDING WHEEL SPEC UNI. MA-60-HV.

WORK PIECE EN 24 ANNEALED.

VPN = 240

EXPERIMENT: COOLANT EFFICIENCY TESTS

RESULTS B = 0.100 INS L = 0.054 INS

REMARKS: E = 0.00042 INS A = 0.14 TO 0.22 SQ. INS

NAME: PURCELL T. CHATER

DATE 96

SURFACE AREA GROUND SQ. INS	WHEEL FACE WIDTH	WHEEL FACE LOSS	SURFACE AREA GROUND	WHEEL FACE WIDTH	WHEEL FACE LOSS
START OF TEST	0.690	NONE	START OF TEST	0.680	NONE
20	0.630	0.060	20	0.590	0.090
40	0.590	0.040	40	0.580	0.010
60	"	NONE	60	"	NONE
80	"	"	80	"	"
100	0.530	0.060	100	0.530	0.050
120	"	NONE *	120	"	NONE *
140	"	"	140	"	"
160	0.500	0.030	160	"	"
182	"	NONE	180	"	"
200	"	"	200	"	"
220	"	"	220	0.490	0.040
240	"	"	240	"	NONE
260	"	"	260	"	"
280	"	"	280	"	"
300	"	"	300	"	"
320	"	"	320	"	"
340	"	"	340	"	"
360	"	"	360	0.440	0.050
380	"	"	380	"	NONE
400	0.430	0.070	400	"	"
420	END OF TEST	NONE	420	END OF TEST	"

DEPTH. OF CUT. = 0.001 in. **Th**
TABLE SPEED. = 65 ft/min.
CROSS. FEED. = 0.042 in./STROKE.

EXPERIMENTAL RECORD

GRINDING WHEEL SPEC UN, TRA 60 HV
NORR PIECE EN 24 ANNEALED.
VPN - 240

EXPERIMENT: COOLANT EFFICIENCY TEST
 RESULTS: B = 0.100 INS. L = 0.054 INS.
 REMARKS: E = 0.00042 INS. A =

NAME J. Purcell T. Chatter

DATE _____ 97

SURFACE AREA. GROUND	AREA, Sq. IN.	WHEEL FACE WIDTH	WHEEL FACE LOSS		SURFACE AREA. GROUND Sq. IN.	WHEEL FACE WIDTH	WHEEL FACE LOSS					
START OF TEST.		0.720	NONE.		440	0.550	NONE					
20		0.670	0.050		460	"	"					
40		0.620	0.050		480	"	"					
60		"	NONE		500	"	"					
80		"	"		520	"	"					
100		"	"		540	"	"					
120		"	"		560	0.520	0.030					
140		"	"		580	"	NONE					
160		"	"		600	"	"					
180		"	"		620	"	"					
200	0.590		0.030		640	"	"					
220	"		NONE *		660	"	"					
240	"		"		680	"	"					
260	"		"		700	"	"					
280	"		"		720	"	"					
300	"		"		740	0.470	0.050					
320	"		"		760	"	NONE					
340	"		"		780	"	"					
360	0.550		0.040		800	"	"					
380	"		NONE.		820	"	"					
400	"		"		840	"	"					
420	"		"		860	0.420	0.050	END OF TEST.				

CONDITIONS

DEPTH OF CUT = 0.001 INS.
TABLE SPEED = 65 FT/MIN
CROSS FEED = 0.042 INS/STROKE

The College of Aeronautics

EXPERIMENTAL RECORD

GRINDING TESTS.

COOLANT SAMPLE No 4

GRINDING WHEEL SPECIFICATION UNI. MA-60-H
WORKPIECE EN 24 ANNEALED.
VPM-240
NAME: PURCELL - T. CHATER.

EXPERIMENT: COOLANT EFFICIENCY TESTS

RESULTS B = 0.1 INS. L = 0.054.

REMARKS: E = 0.00042 INS. A = 0.2 TO 0.23 CUS/INS DATE

G 8

SURFACE AREA GROUND SQ IN.	WHEEL FACE WIDTH	WHEEL WIDTH LOST		SURFACE AREA GROUND	WHEEL FACE WIDTH	WHEEL WIDTH LOST		SURFACE AREA GROUND	WHEEL FACE WIDTH	WHEEL WIDTH LOST
START OF TEST	0.700	NONE		300	0.530	NONE		160	0.620	NONE
20	0.630	0.070	B	320	0.450	0.080		180	"	"
40	0.600	0.030		340	"	NONE		200	0.550	0.070
60	"	NONE		360	"	"		220	"	NONE*
80	"	"		380	"	"		240	"	"
END OF TEST				400	"	"		260	"	"
2ND TEST				420	"	"		280	"	"
START	0.700	NONE		440	"	"		300	"	"
20	0.630	0.080	B	460	"	"		320	"	"
40	0.600	0.100		480	"	"		340	"	"
60	"	NONE		500	"	"		360	"	"
80	"	"		520	"	"		380	"	"
100	0.530	0.070		540	0.400	0.050		400	0.500	0.050
120	"	NONE*		3RD TEST END OF TEST				420	"	NONE
140	"	"		START	0.720	NONE		440	"	"
160	"	"		20	0.640	0.080	B	460	"	"
180	"	"		40	0.620	0.020	0.000 IN	480	"	"
200	"	"		60	"	NONE		500	"	"
220	"	"		80	"	"		520	"	"
240	"	"		100	"	"		540	"	"
260	"	"		120	"	"		560	"	"
280	"	"		140	"	"		580	"	"
CONTINUED				CONTINUED				END OF TEST		

CONDITIONS.

DEPTH OF CUT. = 0.001 INS.

TABLE SPEED. = 65 ft/min.

CROSS FEED. = 0.042 in / STROKE.

The College of Aeronautics

EXPERIMENTAL RECORD

GRINDING TESTS.

EXPERIMENT: COOLANT EFFICIENCY TESTS

R

$$\beta = 0.1 \text{ in}$$
$$L = 0.054$$
REMARKS: $E = 0.00042$
$$A = 0.2 \text{ to } 0.23 \text{ cm}^2/\text{in}^2$$

NAME J. Purcell T. Chatter

DATE _____

99.

COOLANT SAMPLE N^o 4

GRINDING WHEEL UNI. MA. 60 T.Y.
SPECIFICATION.

SPECIFICATION

WORKPIECE EN 24 ANNEALED.

VPN-240.

SURFACE AREA. GROUND. SQ. IN'S	WHEEL FACE WIDTH	WHEEL WIDTH. LOOSE.	SURFACE AREA. GROUND. SQ. IN'S	WHEEL FACE. WIDTH.	WHEEL FACE. LOOSE.
Start of Test.	0.730	NONE.	440	"	"
20	0.660	0.070	460	0.540	0.030
40	0.630	0.030	480	"	NONE
60	"	NONE	500	"	"
80	"	"	520	"	"
100	"	"	540	"	"
120	"	"	560	"	"
140	"	"	580	"	"
160	"	"	600	"	"
180	"	"	620	"	"
200	"	"	640	0.560	0.040
220	"	"	660	"	NONE
240	0.570	0.060	680	"	"
260	"	NONE *	700	"	"
280	"	"	720	"	"
300	"	"	740	"	"
320	"	"	760	"	"
340	"	"	780	"	"
360	"	"	800.	"	"
380	"	"	820	"	"
400	"	"	840	0.450	0.050
420	"	"	End of Test		

The College of Aeronautics

CONDITIONS.

DEPTH OF CUT = 0.001 IN.
TABLE SPEED = 65 FT/MIN.
CROSS FEED = 0.042 IN/STROKE

EXPERIMENTAL RECORD

COOLANT SAMPLE No 4

GRINDING WHEEL SPEC. UNI: MA-60 HV
WORKPIECE EN 24 ANNEALED
VPAI 240

EXPERIMENT: COOLANT EFFICIENCY TESTS

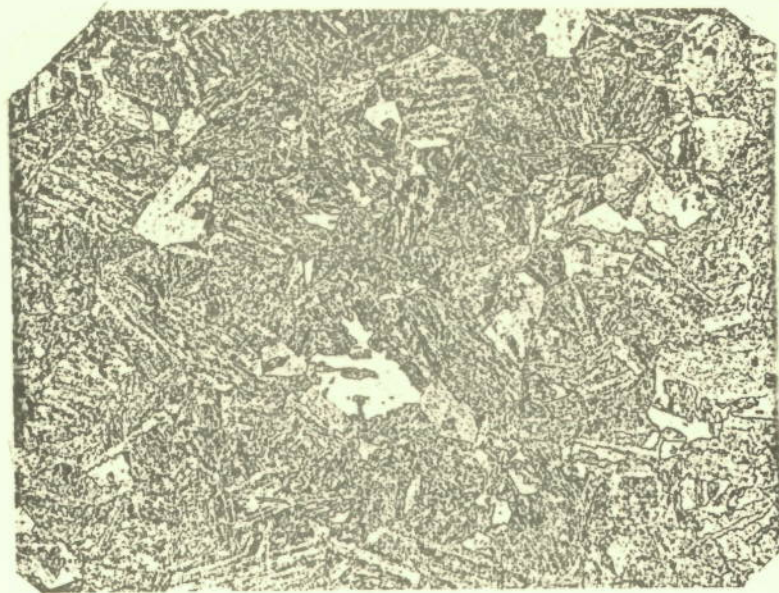
NAME: PURCELL - T. CHATER.

RESULTS B = 0.100 INS L = 0.054 INS

REMARKS: E = 0.00042 INS A = 0.2 TO 0.230²/INS

DATE 9 10

SURFACE AREA GROUND SQ. INS.	WHEEL FACE WIDTH INS.	WHEEL WIDTH LOSS INS.	SURFACE AREA GROUND	WHEEL FACE WIDTH INS.	WHEEL WIDTH LOSS INS.
START of TEST No 4.	0.700	B	NONE	0.450	NONE
20	0.600	0.100 IN	0.100	460	"
40	"	NONE	480	"	"
60	"	"	500	"	"
80	"	"	520	"	"
100	"	"	540	"	"
120	"	"	560	"	"
140	"	"	586	"	"
160	0.510	0.900	600	"	"
180	"	NONE *	620	0.400	0.050
200	"	"	END OF TEST		
220	"	"			
240	"	"			
260	"	"			
280	"	"			
300	"	"			
320	"	"			
340	"	"			
360	0.450	0.060			
380	"	NONE			
400	"	"			
420	CONTINUED				



FIGS. M1 and M2

MICRO AND MACRO STRUCTURE OF THE
WORK PIECE MATERIAL EN 24 IN THE
ANNEALED STATE.

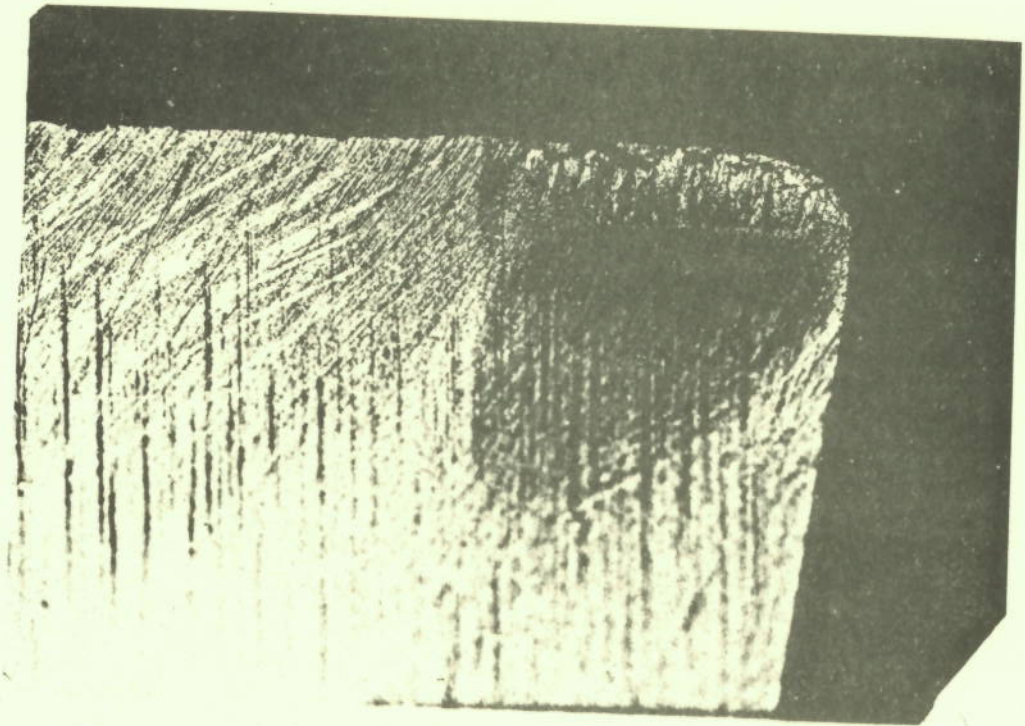


FIG. 2 TYPICAL TOP FACE CRATER
ON TURNING TOOL

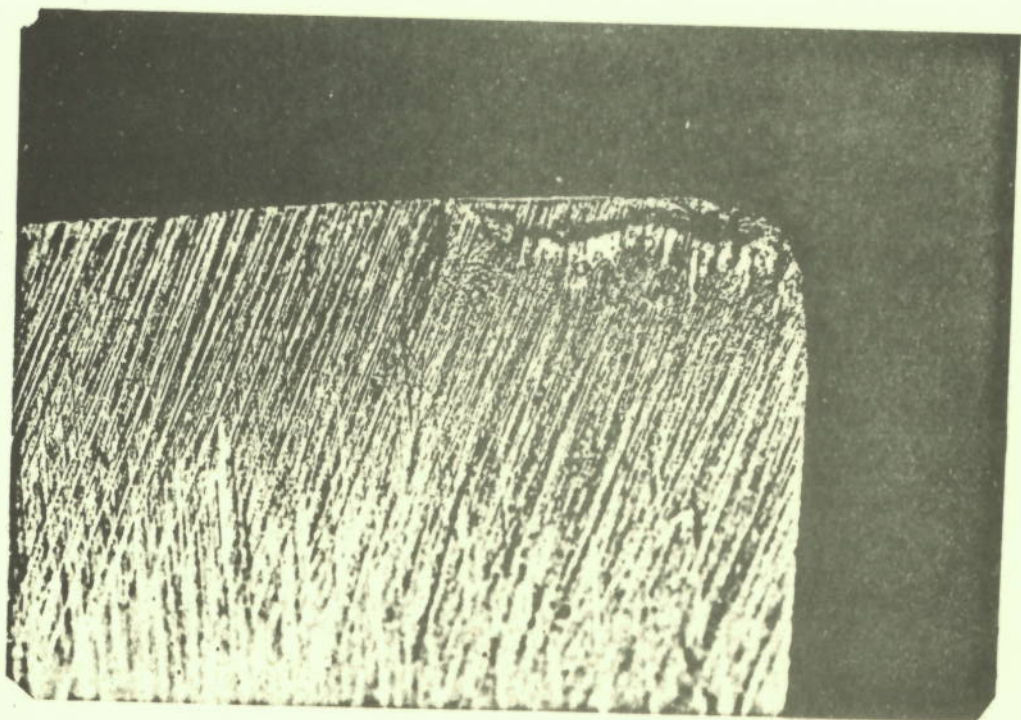


FIG. 3 TOOL FAILING DUE TO
CHIPPING

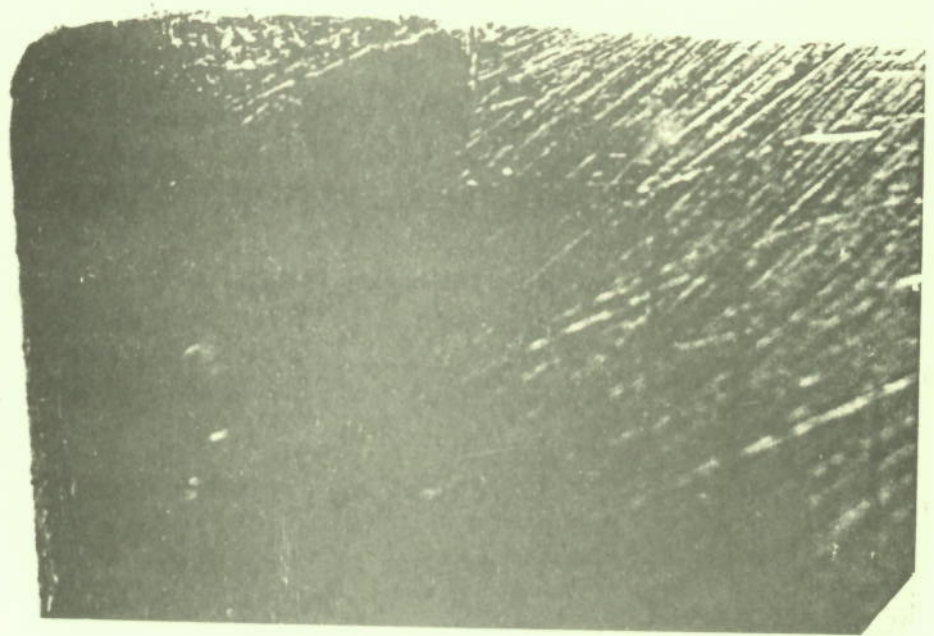


FIG. 4 TYPICAL FLANK AND NOSE
WEAR LAND. THE EXTENT
OF THE WEAR IS CLEARLY
SEEN

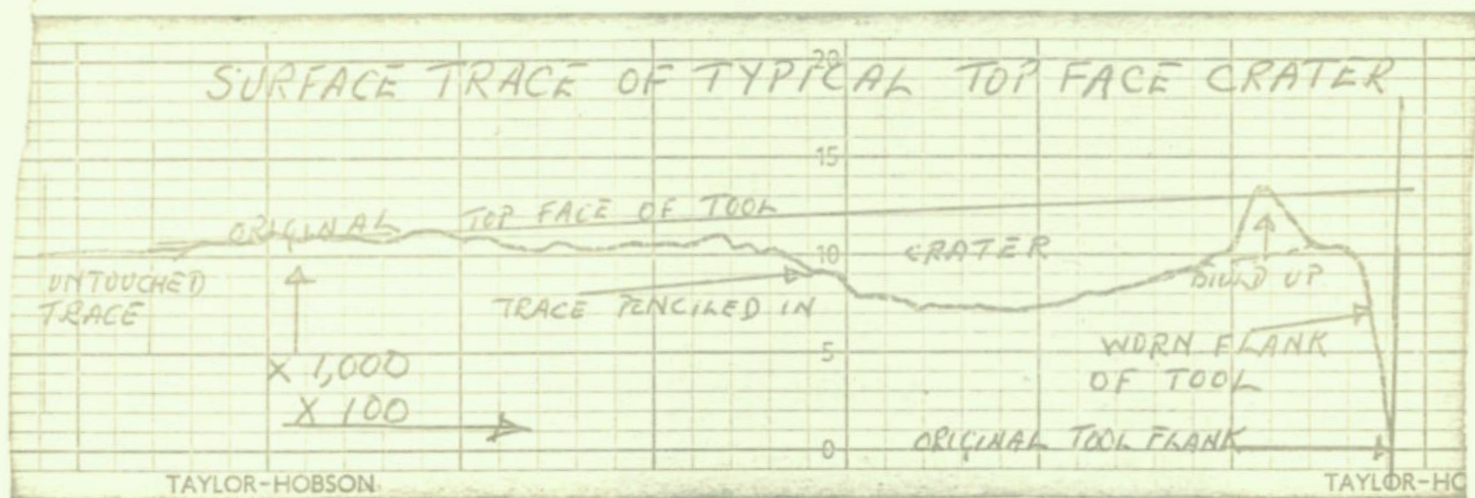
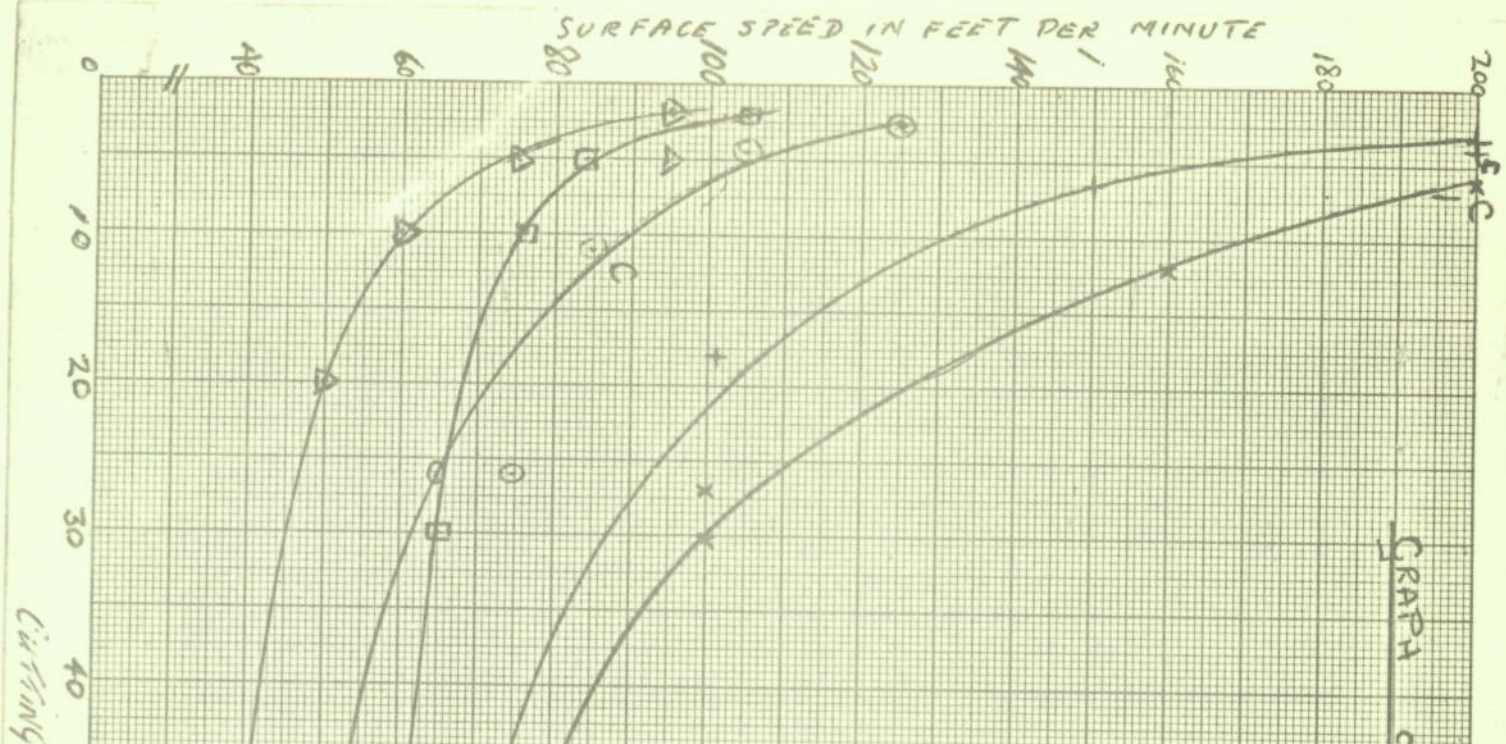


FIG. 5 TALISURF TRACE OF TYPICAL TOP FACE CRATER

R



TURNING TESTS. HSS TOOLS.
GRAPH OF SURFACE SPEED V_s CUTTING TIME
TO 0.018 INS WEAR LAND

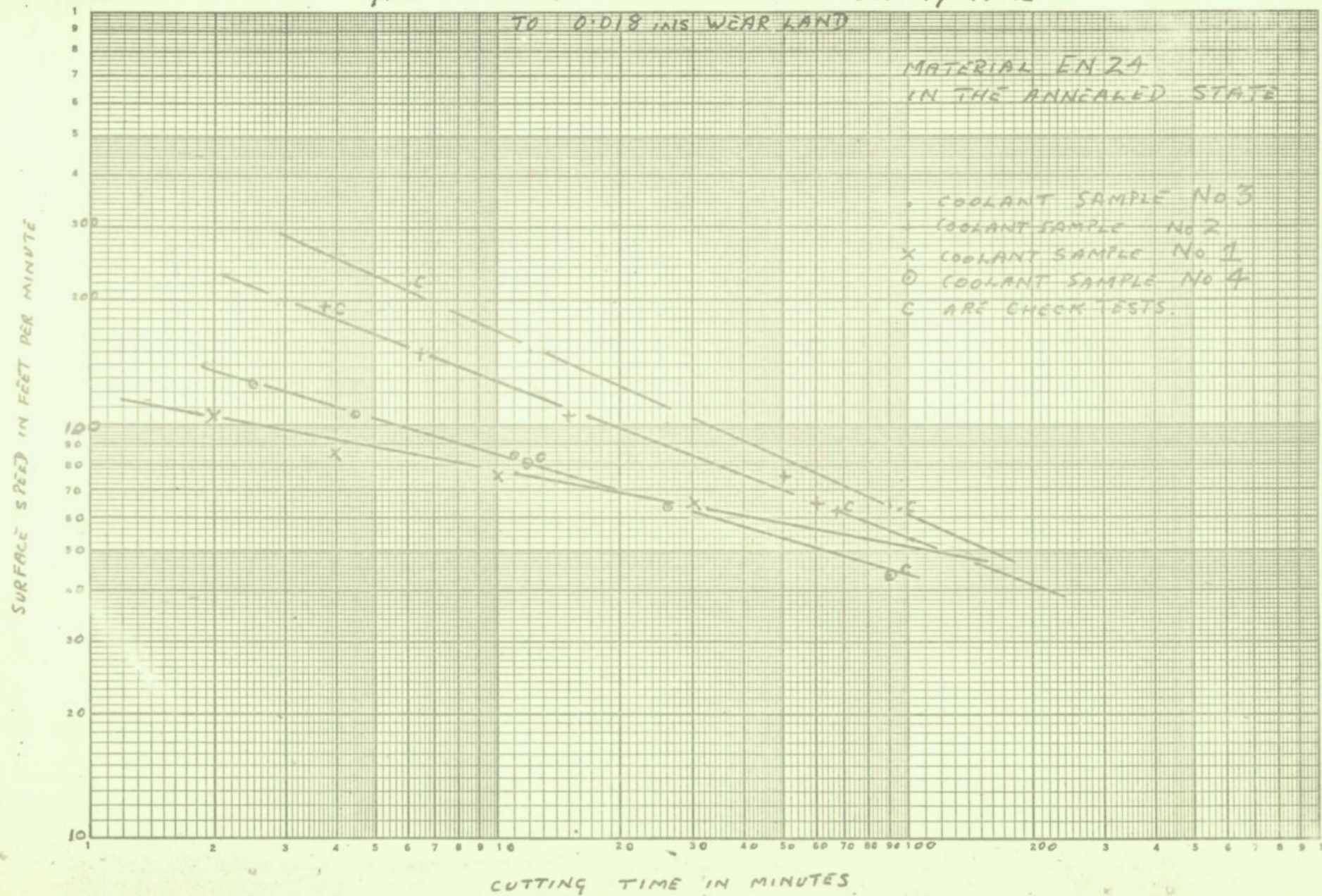


FIG. 6

THE TOOL $\frac{3}{4}$ " DIA. HSS.
SUPPLIED BY
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EXPERIMENTAL RECORD TURNING TESTS.

WORK MATERIAL EN 24 ANNEALED.
VPN 264 AV.

CONDITIONS = DEPTH OF CUT = 0.0100 INS
FEED PER REV = 0.005 INS
TOOK ANGLES CUTTING EDGE SIDE RAKE = 15°
(HSS 1886-1952) PLAN APPROACH ANGLE = 5°
FRONT SIDE CLEARANCE = 6°
PLAN TRAIL ANGLE = 6°
NOSE RADIUS = 0.040 INS.

EXPERIMENT: COOLANT EVALUATION TESTS.

REMARKS: COOLANT SAMPLE No. 1 151.

NAME DATE SURFACE SPEED THE VARIABLE

T1

TOOL No	PLAIN END.	SURFACE SPEED FEET PER MIN.	CUTTING TIME IN MINUTES	FLANK	TOOL WEAR IN INCHES NOSE	CRATER	REMARKS
2.		65	6	0.012	0.014	NONE	SLIGHT CHIP
	CHECK TEST		12	0.013	0.015	"	" "
	TOOK STOPPED		18	0.014	0.015		0.012"
	LESS FREQUENTLY.		24	0.016	0.021?		0.014"
			28	0.017	0.018		CUTTING EDGE FAIRING
			30	0.017	0.019		
No 8	MARKED END.	65.	6	0.010	0.012	NONE	SLIGHT CHIP.
	RECORDED EVERY		12	0.015	0.016		" "
	2 MINUTES.		18	0.016	0.016		CHIP WORN AWAY
	REPRODUCED.		24	0.017	0.016		CHIPPED.
	RECORD 6 MIN		28	0.018	0.018		" worn out.
	INTERVALS.		30	0.020	0.020		NOSE FAIRING
No 8	PLAIN END	65	6	0.015	0.010	NONE	
	19 READINGS.		12	0.017	0.015	"	CHIPPED ON FLANK
	OF WEAR TAKEN		18	0.017	0.015	"	" "
	THESE ARE REDUCED.		24	0.020	0.018	"	second chip
	FOR REPORT		28	0.022	0.020	"	both chips joined
	CLARITY.		32	0.032	0.022	ALMOST FAIRING	CUTTING EDGE CRUMBLING

THE TOOL $\frac{3}{4}$ " DIA HSS
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EASTER BROOK ALCARD LTD
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REF MR R.E. DODD.

The College of Aeronautics VPN 246 AV

WORK PIECE MATERIAL EN 24 ANNEAL

EXPERIMENTAL RECORD

TURNING TESTS

CONDITIONS DEPTH OF CUT = 0.100 INS

FEED PER REV = 0.005 INS

TOOL ANGLES = CUTTING EDGE SIDE RAKE 15°

BSS 1886-1952 PLAN APPROACH ANGLE 5°

FRONT AND SIDE CLEARANCE 6°

PLAN TRAIL ANGLE 6°

NOSE RADIUS 0.040 INS

SURFACE SPEED THE VARIABLE.

EXPERIMENT: COOLANT EVALUATION TESTS

REMARKS: COOLANT SAMPLE NO 1C1

TOOL NO	MARK	END	SURFACE SPEED/FT/MIN	CUTTING TIME MINUTES	FLANK	TOOL WEAR IN INCHES		CRATER	REMARKS
						NOSE			
2			65 FEET	4	004	007		NONE	
				8	010	009		"	
				12	016	013		"	
				18	020	017		"	CHIPPED
				24	022	019		MARKED	
				28	025	022		"	
				30	025	030	FAILED.		
No 4	MARK	END	75 FEET	1	006	006			
				3	010	010			
				6	014	DEEP SCRATCH			
				8	016	WORSE			
				10	018	FAILED			
No 3	MARK	END	105 FEET	$\frac{1}{4}$	006	003			
				$\frac{1}{2}$	006	011			
				$\frac{3}{4}$	007	013			
				1	011	015			
				$1\frac{1}{4}$	012	018			
				$1\frac{1}{2}$	018	020			
				2	028	FAILED.			

THE TOOL $\frac{3}{4}$ " DIA HSS
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The College of Aeronautics

WORK MATERIAL EN 24 ANNEALED

VPN 246.AV.

EXPERIMENTAL RECORD TURNING TESTS

CONDITIONS - DEPTH OF CUT = 0.100 INS
 FEED/REV = 0.005 INS
 TOOL ANGLES = CUTTING EDGE SIDE RAKE 15°
 HSS 1886-1952 PLAN APPROACH ANGLE 5°
 FRONT AND SIDE CLEARANCE 6°
 PLAN TRAIL ANGLE 6°
 NOSE RADIUS .040 INS
 SURFACE SPEED THE VARIABLE

EXPERIMENT: COOLANT EVALUATION TESTS

REMARKS: COOLANT SAMPLE No 1

T3

TOOL No	MARK	END	SURFACE SPEED FT/MIN	CUTTING TIME MINUTES	TOOL WEAR IN INCHES	FLANK	NOSE	CRATER	REMARKS
No 4			75 FEET	1		.004	.006		
				3		.010	.010		
				6		.014	DEEP SCRATCH		CHIPPED
				8		.016	" "	WORSE	
				10		.018	.023		
No 4	PLAIN	END	75 FEET	1		.006	.006		
				3		.012	.010		
				6		.015	DEEP SCRATCH ON NOSE		
				8		.016	" "	WORSE	
				10		.018	FAILED		
No 22	PLAIN	END	85 FEET	1		.006	.008		
				2		.012	.014		CHIPPED
				3		.018	.020		"
				4		.021	.023		
No 22	MARK	END	85 FEET	1		.009	.012		
				2		.013	.014		CHIPPED
				3		.018	.020		CHIPPED
				4		.021	.023		CUTTING EDGE CRUMBLER
No 27	MARKED	END	85 FT.	1		.006	.009		
				2		.010	.013		
				3		.017	.015		
				4		.020	.023		CHIPPED

THE TOOL - HSS $\frac{3}{4}$ " DIA.
 SUPPLIED BY
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EXPERIMENTAL RECORD TURNING TESTS

EXPERIMENT: COOLANT EVALUATION TESTS

REMARKS: COOLANT SAMPLE No 2 1c1

WORK MATERIAL - EN 24 ANNEALED

VPN 246 AV

CONDITIONS - DEPTH OF CUT = 0.100 INS

FEED/REV/REV = 0.005"

TOOL ANGLES - CUTTING EDGE SIDE RAKE 15°
 (BSS 1886) PLAN APPROACH ANGLE 50°
 1952 FRONT AND SIDE CLEARANCE ANGLES 6°

~~DATE~~

PLAN TRAIL ANGLE 6°
 NOSE RADIUS 0.042 INS
~~DATE~~ SURFACE SPEED THE VARIABLE

T4

TOOL NO	PLAIN	END	SURFACE SPEED FEET MIN.	CUTTING TIME IN MINUTES	FLANK	TOOL NOSE	WEAR IN. INS.	CRATER	REMARKS
31			65	5	0.005	0.004			MARKED OUT. SLIGHT SMOKE
				10	0.006	0.006			NICE EVEN FLANK AND NOSE WEAR
				30	0.010	0.009			" "
				40	0.013	0.014			DEEP MARK ON NOSE
				50	0.015	0.014			WEARING MORE RAPIDLY
No				60	0.017	0.018			APPECIABLE SMOKE & SMELL
31	MARKED	END.	75 FT MIN.	2	0.003	0.002			
				6	0.005	0.002			NICE EVEN WEAR
				10	0.007	0.008			ONLY SLIGHT CRATERING
				20	0.010	0.010			SMOKE AND SMELL
				30	0.012	0.013			NOTICABLE.
				40	0.015	0.015			
				50	0.017	0.020			
22	PLAIN	END	150 FT	1	0.003	0.002			
				3	0.010	0.007			CRATERING
				5	0.013	0.010			SMOKE & SMELL INCREASED
				6½	0.015	0.019			NOSE FAILED
22	MARKED	END	105	3	0.006	0.008			SMOKE AND SMELL
				6	0.010	0.008			INCREASED
				9	0.013	0.012			FROM SLOWER SPEEDS.
				12	0.014	0.014			
				15	0.017	0.015			

SLIGHT CRATER.
 CHIPPED

THE TOOL - HSS $\frac{3}{4}$ " DIA.
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EXPERIMENTAL RECORD TURNING TESTS

WORK MATERIAL EN 24 ANNEALED
 VPN 246 AV

CONDITIONS DEPTH OF CUT = 0.100 INS
 FEED/PER/REV = 0.005 INS
 TOOL ANGLES CUTTING EDGE SIDE RAKE 15°
 (BSS 1886-1952) PLAN APPROACH ANGLE = 5°
 FRONT SIDE CLEARANCE ANGLE = 6°
 PLAN TRAIL ANGLE 6°
 NOSE RADIUS 0.040 INS
 SURFACE SPEED THE VARIABLE

EXPERIMENT: COOLANT EVALUATION TESTS

REMARKS: COOLANT SAMPLE No 2 101

T5

TOOL No	PLAIN END	SURFACE SPEED FEET/MIN	CUTTING TIME IN MINUTES	FLANK	TOOL WEAR IN INCHES NOSE	CRATER	REMARKS
26		65	3	0.004	0.002	NONE	SLIGHT
			6	0.004	0.004	"	SMELL & SMOKE
			10	0.007	0.004		SMALL CHIP.
			20	0.008	0.006		CHIP WEARING OUT
			30	0.008	0.013		WENT INCREASED SMOKE WORSE
			40	0.011	0.013		in clipped one
			50	0.013	0.015		
No			60	0.016	0.015		
21	PLAIN END	105 FT	1	0.008	0.006	NONE	(SMOKING)
			3	0.008	0.008		SLIGHT CRATER
			6	0.010	0.009		INCREASE
			9	0.012	0.011		"
			12	0.015	0.011		"
			15	0.016	0.015		CHIPPED
No							
20	MARKED END	150 FT	1	0.005	0.003		CRATER MARKED
			3	0.009	0.007		CRATERING SLIGHT
			5	0.014	0.009		"
			6 1/2	0.014	0.019		DIRECTION OF CHIP FLOW CHANGED
27	PLAIN END	200 FT	1	0.006	0.003		
			2	0.013	0.009		SMOKE AND SMELL
			3	0.011			NOSE FAILED

THE TOOL = HSS - 3/4 DIA.
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 REF. MR R.E. DODD.

The College of Aeronautics

WORK MATERIAL = E.N. 24. ANNEAL.

VPN 246 AV

EXPERIMENTAL RECORD TURNING TESTS

CONDITIONS: DEPTH OF CUT = 0.000 IN

FEED/PER/REV = 0.005 IN

TOOL ANGLES: CUTTING EDGE SIDE RAKE 15°

(BSS 1886-1952) PLAN APPROACH ANGLE 50°

FRONT & SIDE CLEARANCE 60°

PLAN TRAIL ANGLE 60°

NOSE RADIUS = 0.000 IN

~~TOOL~~ SURFACE SPEED THE VARIABLE

EXPERIMENT: COOLANT EVALUATION TESTS

REMARKS: COOLANT SAMPLE No2 ICI.

T6

TOOL No			SURFACE SPEED FT/MIN	CUTTING TIME MINS	FLANK	TOOL WEAR IN INCHES	CRATER	REMARKS
19	PLAIN	END.	65 FT/MIN	3	0.003	0.002		
				6	0.003	0.004		
				10	0.004	0.006		
				20	0.005	0.006	SMOKING	SLIGHTLY
				30	0.008	0.009	CHIPPED	
				40	0.011	0.011	CHIPPED MORE	" "
				50	0.012	0.015	CHIP WEARING OUT	" INCREASED
				60	0.014	0.015	V-GROOVE AT DEPTH OF CUT.	
				70	0.017	0.020	POINT FRAILING.	
No								
19	MARK	END		1	0.002	NONE		SLIGHT
			75 FT	3	0.002	0.002		SMOKE
				6	0.006	0.002		AND
				10	0.006	0.011		SMELL
				30	0.012	0.016	Very slight crater.	
				45	0.017	0.016		
No								
20	PLAIN	END	200 FT	1	0.005	0.005	CRATERING +	SMOKING, SMELL
				2	0.008	0.006	"	"
				3	0.010	0.014	NOSE WEAR.	
				3 1/2			NOSE FAILED.	

THE TOOL $\frac{3}{4}$ " DIA HSS
SUPPLIED BY
EASTERBROOK ALCARD LTD
SHEFFIELD

REF MR R.E. DODD.

EXPERIMENT: COOLANT EVALUATION TESTS

REMARKS: COOLANT SAMPLE NO 3 1C1

The College of Aeronautics

EXPERIMENTAL RECORD TURNING TESTS

WORK PIECE MATERIAL EN24 ANNEALED
VPN 246AV

CONDITIONS: DEPTH OF CUT = 0.100 IN
FEED PER REV = 0.005
TOOL ANGLES: CUTTING EDGE SIDE RAKE 15°
(BSS 1986-1952) PLAN APPROACH ANGLE 5°
FRONT AND SIDE CLEARANCE 6° 6°
PLAN TRAIL ANGLE
NOSE RADIUS 0.040 IN
DATE SURFACE SPEED THE VARIABLE

T7

TOOL NO	MARK	END	SURFACE SPEED FT/MIN	CUTTING TIME IN MINUTES	FLANK	TOOL WEAR IN INCHES	NOSE	CRATER	REMARKS
No 10			65 FEET	6	011		011		
				15	013		014		SOME SMOKE
				30	017		016	DEVELOPING	& SMELL
				60	019		017		
				90	020		018		
No 10	PLAIN	END	65 FEET	6	010		007		
				15	015		012		
				30	017		017		
				60	019		022		
				90	022		FAILED		
No 6	MARK	END	65 FEET	6	011		009		
				15	013		012		
				30	016		015		
				55	018		018		005
				90	020		MOSE	CHIPPED	
No 6	PLAIN	END	65 FEET	6	005		009		
				20	010		009		
				40	013		013		
				65	017		015		
				85	019		018		CUTTING EDGE CHIPPED

THE TOOL $\frac{3}{4}$ " DIA HSS
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The College of Aeronautics VPN 246 AV

WORK PIECE MATERIAL EN 24 ANNEALED

EXPERIMENTAL RECORD

TURNING TESTS

CONDITIONS - DEPTH OF CUT = 0.100 INS
FEED PER REV = 0.005 INS
TOOK ANGLES CUTTING EDGE SIDE RAKE 15°
(ASS 1886-1952) PLAN APPROACH ANGLE 50°
FRONT & SIDE CLEARANCE 60°
PLAN TRAIL ANGLE 60°
NOSE RADIUS 0.040 INS

EXPERIMENT: COOLANT EVALUATION TESTS

REMARKS: COOLANT SAMPLE No 3.151

~~NAME~~ DATE SURFACE SPEED THE VARIABLE

T8

TOOL No	MARK	END	SURFACE SPEED FEET MINUTE	CUTTING TIME IN MINUTES	FLANK	TOOK WEAR NOSE	IN INCHES CRATER	REMARKS
No 23	1		100 FEET	3	006	005		SMOKING
				6	009	008	SLIGHT	SMEAL.
				14	011	013	"	STRONGER THAN
				20	014	015	"	NO 2
				26	016	017	GOOD	PERFORMANCE
No 23	PLAIN	END	150 FEET	2	007	005		
				5	009	009	cratering	SMOKE. SMELL.
				8	013	015	" "	
				11	017	020	DEEP CRATER	
No 14	MARK	END	100 FEET	3	007	003		
				6	009	005		SMEAL
				14	012	010		AND SMOKE.
				20	015	015	GOOD CUTTING ACTION.	
				26	017	016	SLIGHT CRATER.	
No 14	PLAIN	END	150 FEET	1	003	003		
				2	005	005		SMOKE AND SMELL.
				4	006	008		
				6	008	011	GOOD PERFORMANCE	
				9	010	013	slight crater	
				12	016	017	TOO MUCH SMOKE.	

WORK PIECE MATERIAL EN 24 ANNEALED 27
VPN 246AV

CONDITIONS - DEPTH OF CUT = 0.100 INS
FEED PER REV = 0.005 INS

EXPERIMENTAL RECORD
TURNING TESTS
TOOK ANGLES (BSS 1886-1952)
CUTTING EDGE SIDE RAKE 15°
PLAN APPROACH ANGLE 50°
FRONT SIDE CLEARANCE 60°
PLAN TRAIL ANGLE 60°
Nose Radius 0.40 IN

EXPERIMENT: COOLANT EVALUATION TESTS

NAME _____

REMARKS: COOLANT SAMPLE N13101

DATE _____

SURFACE SPEED THE VARIABLE

TOOL NO	MARK	END	SURFACE SIZE		CUTTING TIME		TOOL	WEAR IN INCHES		REMARKS
			FEET	MINUTE	IN	MINUTES		FLANK	NOSE	
No 5			200	FEET	1		006	004		
					2		008	006		CRATERING
					4		012	012		" INCREASING
					6		016	013		(EDGE FAILING AT DEPTH)
					7		019		DEEP SCRATCH (OF CUT SMOKE)	
No 5	PLAIN	END	200	FEET	1		004	003		SMOKE
					3		009	010		
					5		013	011		
					7		018	016		FLANK FAILING
No 28	PLAIN		65	FEET		RUN FOR 90 MINS			GOOD PERFORMANCE	
						019	019		ONLY ORDINARY CRATERING	
(THIS SAMPLE WOULD BE DIFFICULT TO INTRODUCE IN A WORK SHOP DUE TO SMOKE AND STRONG SMELL.)								SEE TAIL SURF TRACE		
								FIG 5. TAKEN FROM		
								THIS TOOL		

THE TOOL $\frac{3}{4}$ DIA HSS
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 SHEFFIELD
 REF MR R.E.DODD.

The College of Aeronautics VPN 246 AV

WORK PIECE MATERIAL K N 24 ANNEALED

T.10

EXPERIMENTAL RECORD (TURNING TESTS)

CONDITIONS. DEPTH OF CUT = 0.100 INS.
 FEED PER REV = 0.005 INS.
 TOOL ANGLES CUTTING EDGE SIDE RAKE 15°
 (HSS 1886-1952) PLAN APPROACH ANGLE 5°.
~~NAME~~ FRONT & SIDE CLEARANCE 60°.
 PLAN TRAIL ANGLE 60°
~~DATE~~ NOSE RADIUS 0.040 INS.
 SURFACE SPEED THE VARIABLE

EXPERIMENT: COOLANT EVALUATION TESTS.

REMARKS: COOLANT SAMPLE No 4.121

TOOL NO	MARK	END	SURFACE SPEED FEET MIN	CUTTING TIME MINS	FLANK	TOOL WEAR IN INCHES	REMARKS
No 7			65 FEET	6	010	011	NONE
				12	015	014	"
				18	017	016	" CHIPPED
				24	018	018	CRATERING
				26	020	021	increased crater.
No 12	PLAIN	END	105 FEET	$\frac{1}{2}$	009	005	
				2	012	008	CRATERING
				3	015	009	"
				$3\frac{1}{2}$	017	015	"
				4	017	016	"
				$4\frac{1}{2}$	022	017	DEEP CRATER
No 15	PLAIN	END	105 FEET	$\frac{1}{2}$	006	010	
				2	010	010	
				3	013	020	CHIP NOSE
				$3\frac{1}{2}$	015	020	CHIP WEARING OUT
				4	015		
				$4\frac{1}{2}$	020		
No 15	MARK	END	125 FEET	$\frac{1}{2}$	015	009	
				1	018	012	CUTTING EDGE
No 10	TEST REPEATED			$1\frac{1}{2}$	020	015	CRUMBLING
	RESULTS SIMILAR.			2	020	018	
				$2\frac{1}{2}$	023	020	

THE TOOL $\frac{3}{4}$ " DIA HSS
 SUPPLIED BY
 EASTERBROOK ALCARD LTD
 SHEFFIELD
 REF MR R.E.DODD.

The College of Aeronautics

WORKPIECE MATERIAL EN 24 ANNEALED
 VP N 246 AV

EXPERIMENTAL RECORD CONDITIONS DEPTH OF CUT = 0.100 INS
 FEED PER REV = 0.005 INS

(TURNING TESTS) TOOL ANGLES CUTTING EDGE SIDE RAKE 15°
 (BSS 1884) NAME (1952) PLAN APPROACH ANGLE 5°

EXPERIMENT COOLANT EVALUATION TESTS

REMARKS COOLANT SAMPLE No 4 101.

FRONT + SIDE CLEARANCE 6°
 PLAN TRAIL ANGLE 6°
 NOSE RADIUS 0.040 INS
 SURFACE SPEED THE VARIABLE

TOOL NO	END	SURFACE SPEED FEET MIN	CUTTING TIME MINS	FLANK	TOOL WEAR IN INCHES NOSE	CRATER	REMARKS
7	MARK	65 FEET	3	003	003	006	
			6	007	007	007	NONE
			12	012	012	009	SLIGHT 0013
			18	014	014	012	CHIP
			24	0	014	017	INCREASING
			26		019	FAILING	
13	MARK END	65 FEET	3	005	005	005	NONE
			6	009	009	009	"
			12	013	013	011	SLIGHT
			18	015	015	013	INCREASED
			24	016	016	013	" NOSE CHIP
			30	018	018	016	"
13	PLAIN END	65 FEET	8	005	005	008	
			16	012	012	013	CRATERING
			24	016	016	014	"
			32	020	020	014	"
No 4	PLAIN END	85 FEET	1	006	006	010	
			3	009	009	010	
TEST REPEATED			6	013	013	013	CRATERING
WITH SIMILAR			8	016	016	015	"
RESULTS			10	017	017	018	INCREASED
			11	021	021	020	

DRILL $\frac{3}{8}$ INS STANDARD JOBBER
 CLEARANCE ANGLE
 HSS PRESTO BRAND

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H.D. 1

EXPERIMENTAL RECORD DRILLING TESTS



VPN
 READINGS

EXPERIMENT: HARDNESS TESTS ON DRILLS

NAME _____

20 KG LOAD

STANDARD VICKERS
 MACHINE

TAKEN ON THE CLEARANCE FACE
 REMARKS: AVERAGE OF 6 READINGS ON EACH FLUTE

DATE _____

PRESTO BRAND DRILLS BY EASTERBROOK ALLCARD SHEFFIELD

DRILL	FLUTE No 1	FLUTE No 2	DRILL	FLUTE No 1	FLUTE No 2
No 1	962	960	No 12	962	959
2	965	952	13	965	949
3	949	952	14	952	949
4	960	945	15	961	937
5	961	968	16	949	965
6	969	952	17	953	956
7	953	946	18	943	978
8	937	939	19	937	937
9	949	951	20	971	959
10	959	962	21	962	962
11	931	931	22	953	949

DRILL $\frac{3}{8}$ " STANDARD JOBBER.

7° FRONT CLEARANCE ANGLE

PRESTO BRAND.

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EXPERIMENTAL RECORD

DRILLING TESTS

D.1.

MATERIAL - EN. 24 ANNEALED

VPN 246.

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME _____

REMARKS: COOLANT SAMPLE ICI No 1

DATE _____

DRILL	VPN	RPM	FEED PER REV	NO OF HOLES DRILLED	DRILL WEAR. IN INCHES	REMARKS	
No	971	920	IN INS.	IN DEEP.	CORNERS CHISEL POINT		
20	959		.007	10	.002 .003 .006 .004	GOOD CLEAN	
				20	.002 .005 .008 .008	PERFORMANCE	
				40	.004 .007 .009 .011		
				60	.007 .008 .016 .017		
				80	.008 .010 .018 .019		
				100	.009 .010 FAILED.		
20	974		2nd run after redress				
	964			10	.004 .003 .003 .005		
				20	.004 .006 .008 .009		
				30	.005 .006 .009 .011	AT 100 HOLES	
				40	.006 .006 .010 .011	PERFORMANCE	
				50	.006 .007 .013 .012	IS BETTER	
				60	.007 ^{CHIPPED} .013 .016	THAN. NO 3	
				70	.008 .008 .014 .016		
				80	.008 ^{CHIPPED} .017 .020		
				90	.013 .010 .017 .020		
				100	.016 .014 FAILED.		

DRILL $\frac{3}{8}$ " DIA STANDARD TOBBER The College of Aeronautics

Y° FRONT CLEARANCE ANGLE

PRESTO. BRAND

EXPERIMENTAL RECORD
DRILLING TESTS

MATERIAL EN 24 ANNEALED
VPN 246.

D. 2

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME _____

REMARKS: COOLANT SAMPLE ICI No. 1

DATE _____

DRILL	VPN	RPM	FEED PER REV	NO OF HOLES DRIILLED	DRILL WEAR IN INCHES	REMARKS
No			IN INS	1 INS DEEP	CORNERS CHISEA POINT	
20	964	920	.007	10	.004 .002 .003 .003	
				20	.005 .004 .005 .006	
				30	.006 .008 .006 .006	GOOD CLEAN
				40	.008 .010 .010 .006	PERFORMANCE AND
				50	.010 .012 .011 .006	STEADY RATE OF W
				60	.012 .012 .012 .010	WEAR.
				70	.012 .013 .012 .012	
				80	.013 .014 CHIPPED .018	
				100	.017 .014 CHIPPED CHIPPED.	
2nd run new drill						
No 12	931			10	.003 .002 .003 .002	
	931			20	.004 .004 .006 .006	
				30	.006 .008 .007 .011	
				40	.008 .010 .008 .014	
				50	.008 .010 .009 .016	
				60	.009 .010 .010 .017	
				70	.009 .014 .010 .018	
				80	.010 .014 .015 .018	
				90	.013 .014 .015 .019	
				100	CHIPPED .018 worn right across	

D.3.

DRILL $\frac{3}{16}$ IN DIA STANDARD JOBAER) **The College of Aeronautics**

7° FRONT CLEARANCE ANGLE.
PRESTO BRAND

EXPERIMENTAL RECORD
DRILLING TESTS

MATERIAL EN 24 ANNEALED.
VPN 246.

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME

REMARKS: COOLANT SAMPLE No 1. ICI.

DATE

DRILL	VPN	RPM	FEED PER REV	No OF HOLE'S DRILLED	DRILL WEAR IN INCHES	REMARKS
No			IN INS	INS FEED	CORNERS CHISEL POINT	
12	938	920				
	932		.007	10	.002 .003 .003 .003	
				20	.002 .003 .008 .008	
				30	.003 .004 .009 .010	
				40	.004 .005 .009 .011	GOOD CONSTANT
				50	.005 .005 .013 .012	
				60	.007 .007 .016 .017	RESULTS.
				70	.008 .008 .018 .019	
				80	.008 .008 .018 .020	Pressure
				100	.009 .010 WORN ACROSS .025	factor
17	946		2nd run after redress			
	936			10	002 003 003 002	
				20	002 003 007 003	
				30	004 003 009 006	
				40	004 005 009 008	
				50	004 006 010 011	
				60	005 006 013 011	
				70	006 007 016 012	
				80	006 007 017 013	
				90	007 008 017 013	
				100	010 011 017 CHIPPED.	

D.4.

DRILL $\frac{3}{8}$ " DIA STANDARD JOBBER

7° FRONT CLEARANCE ANGLE

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EXPERIMENTAL RECORD

DRILLING TESTS

MATERIAL - EN 24 ANNEALED

VPN 246.

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME _____

REMARKS: COOLANT SAMPLE ICI NO 2

DATE _____

DRILL No	VPN	RPM	FEED PER REV IN INS	NO OF HOLES DRILLED 1 IN DEEP	DRILL IN INCHES CORNERS	WEAR CHISEL POINT	REMARKS
11	946	920	.007	10	.004 .004	CHIPPED	
				20	.005 .005	"	
				30	.005 .009	"	
				40	CHIPPED .007	CHIPPED	TEST RESTARTED.
16.	998		restart	after redress			
	968			10	.003 .004	.004 .007	
				24	.003 .006	.007 .008	
				40	.007 .006	.008 .010	
				60	.013 .010	.010 .011	
				70	.015 .011	.010 .013	
				73	CHIPPED	FAILED	
16.	946.		drill	redressed.			
	976			10	.003 .002	.004 .003	
				20	.003 .004	.004 .006	
				40	.005 .004	.008 .007	
				60	.007 .005	.009 .007	
				65	.008 .005	.009 .010	
				70	.014 .010	.014 .016	
				75	.019 .010	FAILED .019	

DRILL $\frac{3}{8}$ " DIA. STANDARD JOBBER

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D.6.

7° CLEARANCE ANGLE

EXPERIMENTAL RECORD

MATERIAL - EN 24 ANNEALED

H.S.S. PRESTO BRAND.

DRILLING TESTS

VPN 246.

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME

REMARKS: COOLANT SAMPLE ICI No.2

DATE

DRILL	VPN	RPM	FEED	NO OF	DRILL	WEAR	REMARKS
No			PER REV	HOLES	IN INCHES		
				DRILLED			
			IN INS	1 INS DEEP	CORNERS	CHISEL POINT	
17	944	920		10	.003 .002	.005 .005	
	942		.007	20	.006 .011	.010 .005	
				40	.013 .011	.011 .006	
				60	.014 .014	.017 .011	
				80	DRILL FAILED	POINT FAILED	
		2nd run after redress			same drill		
17	944	CONSTANT		10	.002 .004	.003 .005	
	942			20	.003 .005	.006 .008	
				30	.004 .005	.007 .010	
				40	.004 .006	.010 .011	
				50	.004 .008	.012 .015	
				60	.005 .008	.015 .017	
		DRILL VIBRATING		70	.009 CORNER	.019 .019	
		UNDER HEAVY FORCES		80	FAILED		
No 16	488	3rd run			NEW drill		
	946			20	.005 .006	.006 .005	
				40	.013 .008	.011 .006	
				60	.014 .010	.015 .017	
				80	.019 .021	FAILED FAILED	

DRILL $\frac{3}{8}$ " STANDARD JOBBER.
7° FRONT CLEARANCE ANGLE

H.S.S.
PRESTO BRAND

EXPERIMENT: COOLANT EFFICIENCY TESTS

REMARKS: COOLANT SAMPLE No 3 ICI

The College of Aeronautics

EXPERIMENTAL RECORD DRILLING TESTS

MATERIAL - EN 24 ANNEALED
VPN 246.

NAME _____

DATE _____

DRILL	VPN	RPM	FEED PER REV	NO OF HOPES DRILLED	DRILL WEAR IN INCHES	REMARKS
No 2	946	920	IN. INS	1 IN. DEEP	CORNERS CHISEL POINT	
	956		.007	10	.004 .002 .006 .003	
				20	.005 .006 .006 .012	
				40	.007 .008 .012 .015	
				60	.007 .008 .018 .017	THE DRILL IS MORE HEAVY LOADED WITH THIS COOLANT THAN WHEN COOLANT No 1 IS USED
				80	.009 .016 .018 .017	
				100	.010 .016 .019 .023	
			2nd run new drill			
No 7	940			10	.002 .004 .006 .003	
	936			20	.004 .005 .009 .004	
				40	.004 chipped .025	
				60		
				80	TEST DISCONTINUED	
				100		
No 7	940		Drill redressed.			
	936			10	.004 .002 .003 .006	
				20	.004 .008 .006 .006	
				40	.006 .008 .006 .006	
				60	.007 .009 .007 .008	
				80	.010 .009 .007 .009	
				100	.032 .014 .010 .015	

DRILL $\frac{3}{8}$ " STANDARD JOBBER.
T° CLEARANCE ANGLE.

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EXPERIMENTAL RECORD DRILLING TESTS

MATERIAL - EN 24. ANNEALED
VPN 246

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME _____

REMARKS: COOLANT SAMPLE NO 3 ICT

DATE _____

DRILL	VPN	RPM	FEED PER REV	No OF HOLES DRILLED	DRILL WEAR IN INCHES	REMARKS
No	936	920	IN INS	1 IN DEEP	CORNERS CHISEL POINT	
2	965		.007	10	.002 .003 .002 .005	
				20	.002 .006 .010 .007	
				40	.004 .007 .013 .013	THE PERFORMANCE
				60	.006 .007 .014 .014	OF THIS COOLANT
				80	.008 .008 .014 .014	IS NOT EQUAL
				100	.009 .010 .018 .015	TO COOLANT
			2nd run after redress			No 1
No 2	965			10	.003 .003 .010 .005	THE PROCESS
	945			20	.006 .004 .010 .005	IS MUCH MORE
				40	.007 .006 .011 .012	HARSH.
				60	.010 .007 .013 .015	
				80	.013 .007 .016 .016	
				100	.014 .010 .018 .017	
No 16	988		redressed drill			
	946.			10	.002 .004 .008 .002	
				20	.004 .006 .008 .007	
				30	.004 .006 .008 .009	
				40	.008 .009 .010 .010	
				60	.008 .012 .011 .011	
				80	.012 .012 .011 .015	
				100	Test ended due to heavy forces	

DRILL $\frac{3}{8}$ " STANDARD JOBBER
 7° CLEARANCE ANGLE
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EXPERIMENTAL RECORD DRILLING TESTS

MATERIAL - EN24 ANNEALED
 VPN 246.

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME _____

REMARKS: COOLANT SAMPLE NO 3

DATE _____

DRILL No	VPN	RPM	FEED PER REV	No OF HOLES DRILLED	DRILL WEAR IN INCHES	R	REMARKS
15	953	920	IN INS	1 INS DEEP	CORNERS CHISEA POINT		
	946		.007	10	.002 .005 .003 .003		
				20	.005 .005 .007 .007		
				40	.005 .006 CHIPPED .008 .009		
				60	.012 .009 .013 .010		PROCESS SOUNDS
				80	.012 .009 .013 .012		HARSH
				100	.019 .012 .017 .012		
			2nd run	after redress			
15	969			10	.006 .002 .003 .002		
	946			20	.012 .003 .005 .007		
				40	.012 .017 CHIPPED		
				60	TEST DISCONTINUED		
			3rd run	after redress			
15	946			10	.002 .004 .003 .002		
	956			20	.006 .004 .006 .004		
				40	.007 .004 .007 .007		
				60	.007 .008 CHIPPED .009 .013		
				80	.012 .010 .009 .015		
				100	.012 .013 .009 .016		

DRILL ⁷/₈ BINS STANDARD JOBBER
7° FRONT CLEARANCE ANGLE
H.S.S

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EXPERIMENTAL RECORD

DRILLING TESTS

MATERIAL - EN. 24. ANNEALED!

VPN 246

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME _____

REMARKS: COOLANT SAMPLE ICI No 4

DATE _____

DRILL No	VPM	RPM	FEED PER REV IN INS.	NO OF HOLES DRILLED 1 INS DEEP	DRILL WEAR IN INCHES				REMARKS
					CORNERS	CHISEL	POINT		
18	937	920	.007	10	.003	.004	.002	.003	
	949			20	.004	.006	.002	.006	
				30	.007	.009	.003	.006	
				40	.007	.010	.006	.009	
				50	.014	.012	.008	.009	AFTER 50 HOLES
	DRILL VIBRATING	60		.018	.014	.012	.015	RATE OF WEAR	
	CUTTING FORCES VERY HIGH	70		.028	.016	.012	.015	INCREASED	
Second run after redress of used drill									RAPIDLY IN ALL
No 16	988			10	.003	.004	.006	.002	TEST WITH THIS
	974			20	.003	.006	.006	.005	COOLANT
				30	.004	.008	.007	.005	
				40	.005	.010	.008	.007	
				50	.006	.014	.011	.008	
				60	.008	.015	.011	.012	
	DRILL VIBRATING	70	.011	.021	.017	.012			
CUTTING FORCES VERY HIGH	76	.018	.028	.017	FAILED				

DRILL $\frac{3}{8}$ STANDARD JOBBER
7° FRONT CLEARANCE ANGLE

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D. 11

MATERIAL-EN. 24 ANNEALED
VPN 246.

EXPERIMENTAL RECORD
DRILLING TESTS

EXPERIMENT: COOLANT EFFICIENCY TESTS

NAME

REMARKS: COOLANT SAMPLE ICI No 4

DATE _____

DRILL No	VPN	RPM	FEED PER REV IN INS	No OF HOLES DRILLED 1. INS DEEP	DRILL WEAR IN INCHES CORNERS CHISEL POINT	REMARKS
16	988					
	946	920	007	10	.003 .008 .002 .003	
				20	.004 .009 .003 .003	
				30	.006 .011 .003 .004	
				40	.011 .014 .006 .004	
				50	.013 .015 .006 .006	
			NEAR FAILURE	60	.016 .017 .009 .014	
			DRILL VIBRATING	69	.018 .021 .009 .017	
			Second run after redress of used drill			
No 14	943			10	.002 .003 .006 .004	
	978			20	.003 .005 .008 .005	
				30	.007 .005 .011 .005	
				40	.007 .066 .011 .006	
				50	.012 .011 .011 .010	
				60	.017 .015 .019 .010	
				70	.021 .019 FAILED.	

DRILL $\frac{3}{8}$ DIA STANDARD JOBBER.

7° FRONT CLEARANCE ANGLE

H.S.S.

PRESTO BRAND

EXPERIMENT: COOLANT EFFICIENCY TESTS

REMARKS: COOLANT SAMPLE ICI No 4

The College of Aeronautics

EXPERIMENTAL RECORD

DRILLING TEST.

D. 12.

MATERIAL - EN 24 ANNEALED
VPN 246

NAME _____

DATE _____

DRILL No	VPN	RPM	FEED PER REV IN. INS.	No OF HOLES DRILLED INS. DEEP.	DRILL WEAR IN INCHES.				REMARKS
					CORNERS	CHISEL POINT			
15	946	920	.007	10	.006	.003	.002	.002	
				20	.007	.008	.006	.003	
				30	.008	.010	.006	.003	
				40	.010	.012	.009	.005	
				50	.017	.016	.013	.008	
				60	.020	.018	.015	.011	
				70	.038	.042	.015	.019	
Second run after redress of used drill									
No 16	988			10	.004	.005	.002	.002	
	946			20	.005	.005	.004	.005	
				30	.005	.006	.005	.006	
				40	.006	.007	.008	.006	
				50	.012	.011	.015	.006	
				60	.014	.012	.017	.008	
				70	.015	.017	.018	.009	

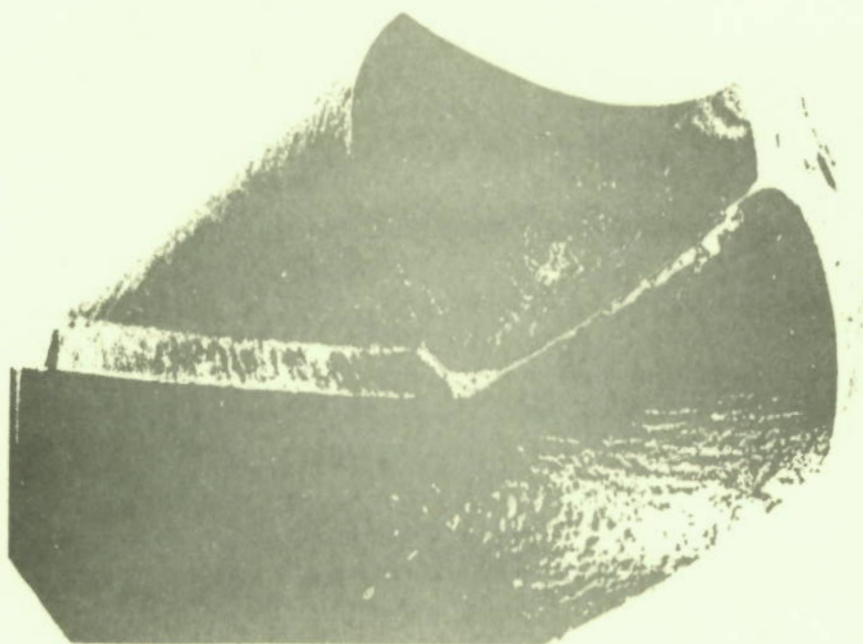


FIG. 8 TYPICAL DRILL RADIAL
CORNER WEAR

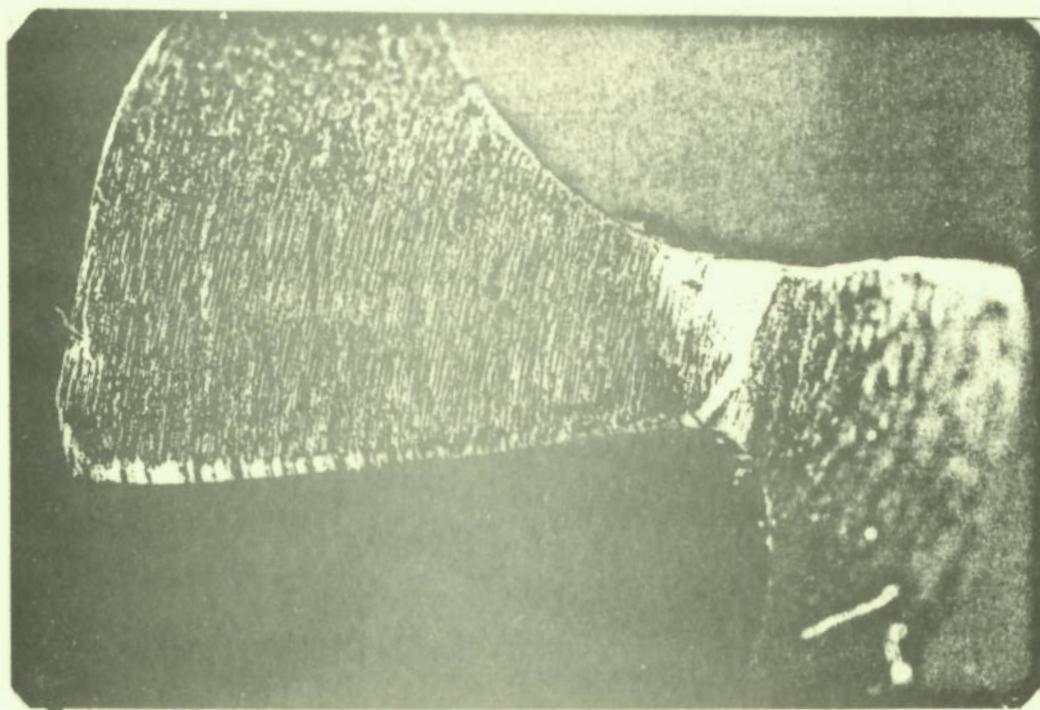


FIG. 9 TYPICAL DRILL CUTTING
EDGE WEAR

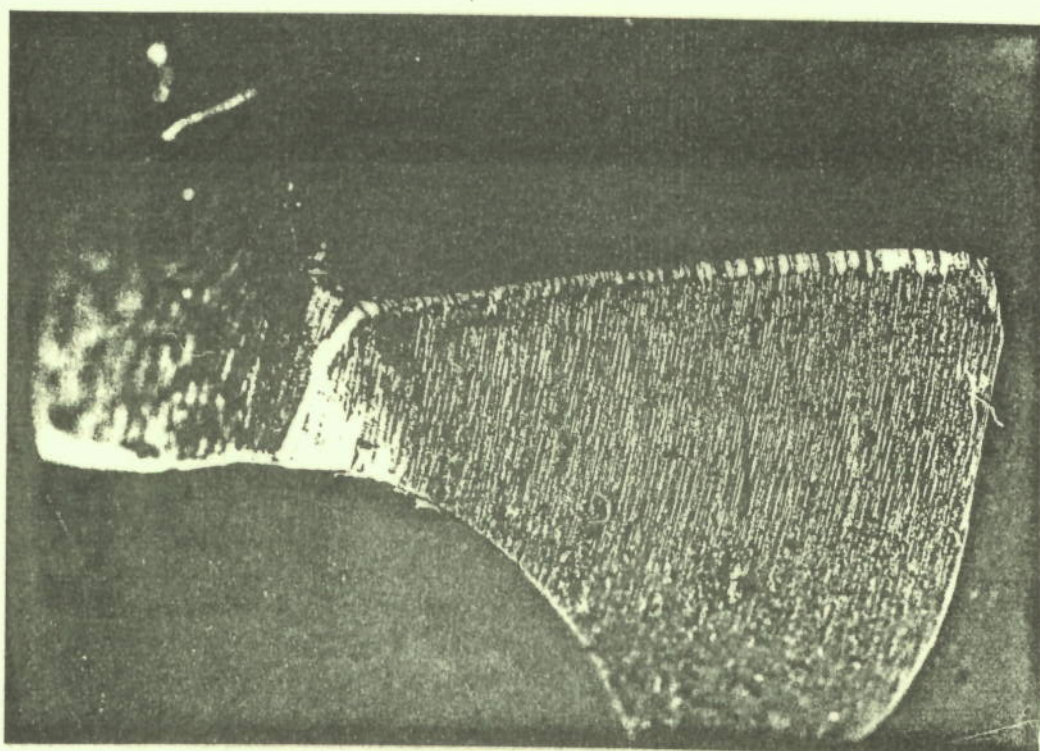


FIG. 10 PHOTOGRAPH OF CHISEL POINT FAILURE