



Unifying nucleation and crystal growth mechanisms in membrane crystallisation

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ABSTRACT

While several mechanisms have been proposed to describe crystallisation processes in membrane distillation, it has not been possible to provide a definitive description since the nucleation kinetics are difficult to measure. This study therefore introduced non-invasive techniques to measure induction time within two discrete domains (the membrane surface and bulk solution) and was complemented by the introduction of a modified power law relation between supersaturation and induction time, that enables mass and heat transfer processes in the boundary layer to be directly related to classical nucleation theory (CNT). Temperature (T , 45–60 °C) and temperature difference (ΔT , 15–30 °C) were used to adjust boundary layer properties, which established a log-linear relation between the nucleation rate and the supersaturation level in the boundary layer at induction, which is characteristic of CNT. Crystal size distribution analysis demonstrated how nucleation rate and crystal growth rate could be adjusted using ΔT and T respectively. Consequently, ΔT and T can be used collectively to fix the supersaturation set point within the boundary layer to achieve the preferred crystal morphology. However, at higher supersaturation levels, scaling was observed. Discrimination of the primary nucleation mechanisms, using measured induction times, revealed scaling to be formed homogeneously, which indicates exposure of the pores to extremely high supersaturation levels. Morphological analysis of scaling indicated growth to be dominated by secondary nucleation mechanisms, that resulted in a habit that is distinctive from the crystal phase formed in the bulk solution. From this analysis, a critical supersaturation threshold was identified, below which kinetically controlled scaling can be ‘switched-off’, leaving crystals to form solely in the bulk solution comprising the preferred cubic morphology. This study serves to unify understanding on nucleation and growth mechanisms to enhance control over crystallisation in membrane systems.

1. Introduction

Crystallisation is an important unit operation for the production of solids in numerous sectors (e.g., pharmaceutical, environment and manufacturing), and is emerging as a critical unit process for the management of desalination brines in the transition toward zero liquid discharge (ZLD) [1]. For crystallisation to occur, the concentration of the solution must exceed the solubility limit to generate a supersaturated solution [2]. It is the extent of supersaturation that is achieved at nucleation which determines the kinetics of nucleation and crystal growth. While crystallisation has been used at an industrial scale to produce and separate valuable solid (crystalline) products from aqueous solutions for many decades [1,3,4], reactor geometries often comprise

poorly-defined interfacial area, which results in poor mixing conditions. Consequently, precise control of heat and mass transfer is difficult to achieve leading to inconsistent regulation of supersaturation, which can introduce wide crystal size distributions (CSDs) with irreproducible product morphology and purity [3]. These properties are important for simplifying downstream recovery, limiting postprocessing requirements, and can be relevant in the final application of the crystalline product [2,5]. It is therefore critical to achieve strict control over supersaturation.

Membrane distillation crystallisation (MDC) concentrates the feed solution by establishing a vapour-pressure gradient across a hydrophobic microporous membrane [2]. The well-defined membrane area facilitates uniform heat and mass transfer, enabling the rate of vapour

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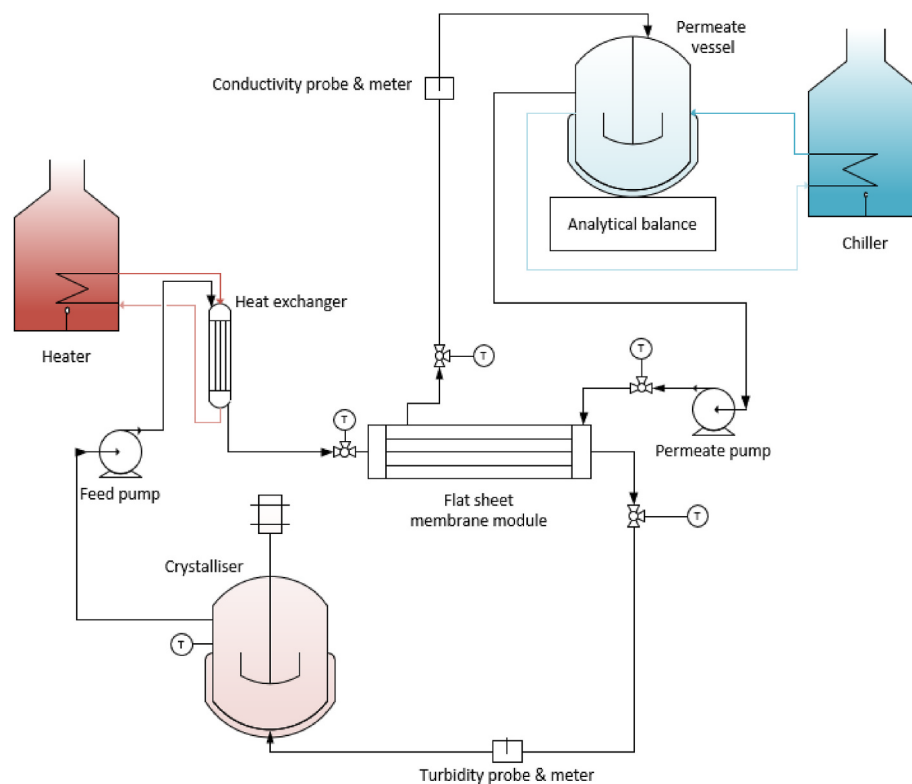


Fig. 1. Schematic of MDC experimental setup.

transfer across the membrane to be precisely controlled. This advances the regulation of supersaturation, therefore improving control over the kinetics of nucleation and crystal growth [2,3,6]. The laminar conditions in the feed channel also promote localised temperature and concentration polarisation phenomena to foster a highly-supersaturated boundary layer [4]. Consequently, it is proposed that nucleation and crystal growth may be independently controlled by the development of two distinct regions; an interfacial boundary layer, where nucleation is most likely to occur, and the bulk solution, where crystal growth can subsequently proceed [7,8]. This was recently illustrated through a characterisation of mixing within these discrete domains which could be correlated to the regulation of nucleation and growth of the crystal phase in the bulk solution [9,10].

Heterogeneous primary nucleation is presumed to be the predominant crystallisation pathway in MDC, as it is proposed that the interfacial energy of the membrane lowers the critical energy barrier for nucleation. However, this reduction in the energy barrier has also been linked to the promotion of scale formation at the membrane, where the ensuing surface coverage leads to a rapid decline in flux [11–13]. Classical nucleation theory can be used to describe both scaling and crystallisation. In both cases, nucleation is assumed to proceed on condition that the change in Gibbs free energy of the system (ΔG) exceeds the critical energy barrier for homogeneous nucleation ($\Delta G > \Delta G_{hom}^*$) or that the energy barrier is sufficiently reduced such that ΔG can overcome the activation energy barrier for heterogeneous nucleation ($\Delta G > \Delta G_{het}^*$) [2,14,15]. An increase in scaling has been observed when temperature difference (ΔT) is increased, which is commensurate with a higher interfacial supersaturation level [12,16]. Various MD studies have also identified greater scaling with an increase in feed temperature which will also raise the maximum saturation level at which scaling occurred [12,16,17]. According to CNT, since supersaturation is the driving force for crystallisation, higher supersaturation levels initiated through an increase in T or ΔT should favour homogeneous nucleation rather than surface (heterogeneous) nucleation [18]. The apparent disconnection between theory and observation cannot be resolved

without determining the supersaturation level at induction and the induction time as these measurements can be used to characterise primary nucleation and delineate between heterogeneous and homogeneous nucleation mechanisms. Misinterpretation of the preferential primary nucleation mechanism may also arise due to the deposition of crystals formed within the bulk solution which can be mistaken as scaling formed through a heterogeneous mechanism. This was illustrated previously for calcium sulphate, where negligible surface scaling was evidenced provided crystals were separated from the bulk solution via filtration [17,19]. Membrane flux has been primarily used as a surrogate measure of induction time, where the inflection point at which the permeate flux drastically declines is used to indicate the onset of crystallisation [6,16,17]. However, this flux decline has been attributed to deposition [9] and therefore cannot provide a representative induction time for nucleation. To advance knowledge of crystallisation in MD, it is therefore critically important to employ techniques that can provide more accurate determination of induction time and enable the delineation of scaling from that of the crystal phase emanating from the bulk solution.

While supersaturation is recognised to be the driving force for crystallisation, the extent of supersaturation that develops within the boundary layer and bulk solution are rarely characterised in MD [9]. The metastable zone width (MSZW) describes the maximum supersaturation ($c-c^*$) achieved by a system at the commencement of nucleation. Through modifying the supersaturation rate (the rate at which a system crosses the metastable zone) and saturation temperature, different levels of supersaturation can therefore be achieved. This will determine the kinetics of nucleation and crystal growth. In MDC, crystallisation behaviour is generally examined through changes to temperature and temperature difference (ΔT) which will simultaneously alter mass and heat transfer processes, subsequently modifying membrane flux and adjusting the metastable zone width. While membrane flux is often used as an empirical measure to infer how system modifications affect crystallisation, it is a normalised parameter that cannot be related to nucleation kinetics as it does not directly describe factors such as solvent

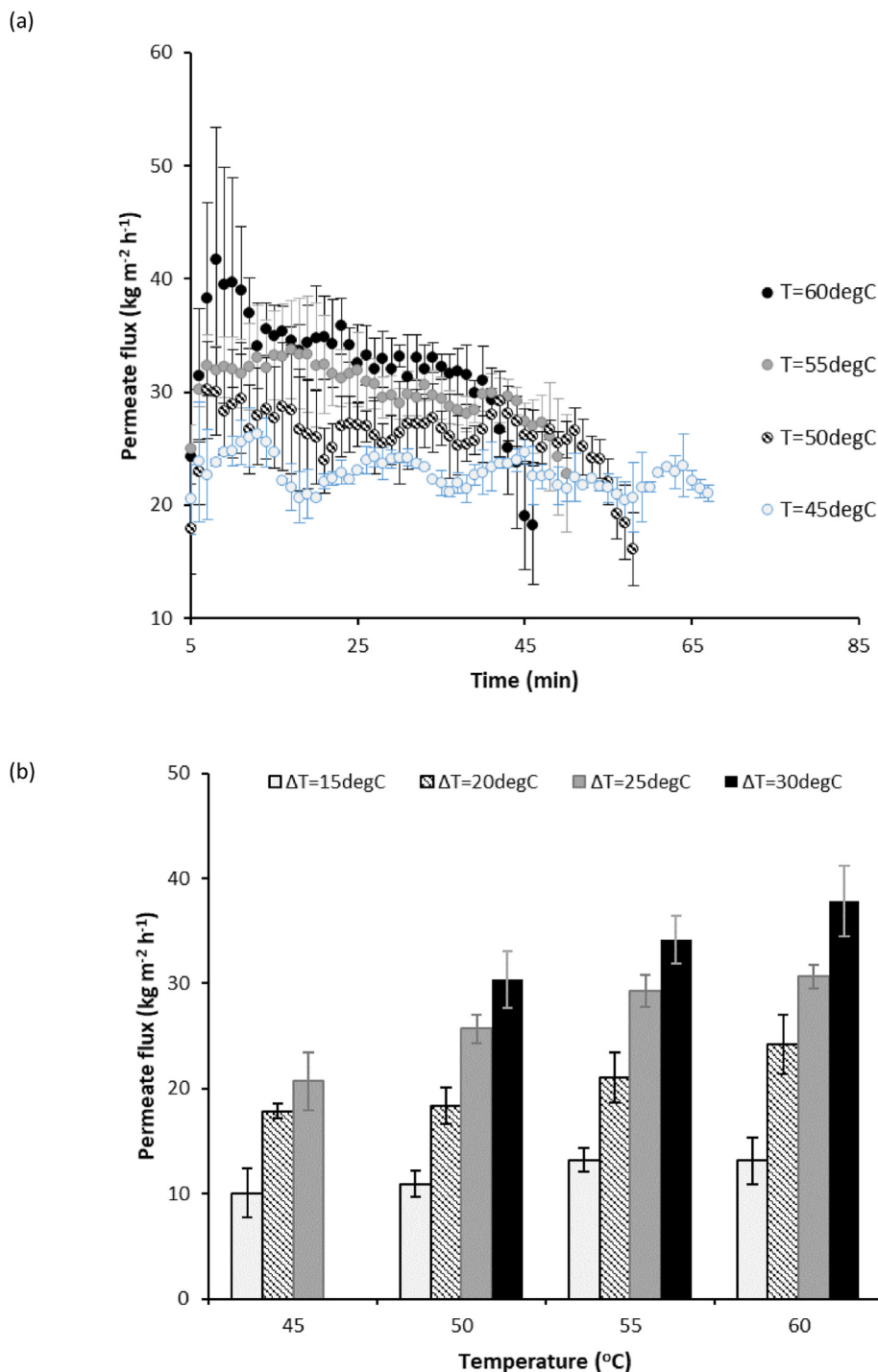


Fig. 2. Determining how temperature (T) and temperature difference (ΔT) modify permeate flux (5-min running average): (a) Illustrative primary data where flux decline is observed (T 45–60 $^{\circ}\text{C}$; ΔT 25 $^{\circ}\text{C}$); and (b) permeate flux at the onset of bulk nucleation based on turbidity response for all experimental conditions (T 45–60 $^{\circ}\text{C}$; ΔT 15–30 $^{\circ}\text{C}$). Error bars indicate standard deviation of at least three replicated experiments undertaken at the same conditions.

volume, solvent removal rate, solute concentration and solvent temperature which are critical to the characterisation of the MSZW [20,21]. The supersaturation rate (R') has therefore been developed to collectively describe these interrelated factors, together with the effects of concentration and temperature polarisation, in a single term, enabling MDC operating parameters to be directly correlated to nucleation rate through classical nucleation theory (CNT) [9]. The application of this term was illustrated when examining how Reynolds number in the feed channel modified the MSZW, but the role of temperature and ΔT were not examined in detail.

In this study, we therefore systematically characterise the kinetics of nucleation and crystal growth when mass and heat transfer processes are modified in MDC by temperature and ΔT to provide a rational basis for crystallisation design. Through a modified Nývlt [22] like approach, the supersaturation rate (R'), which is used to represent MDC operating conditions, provides a direct analogy to nucleation rate. This yields a unifying approach where the power-law relation between nucleation kinetics of sodium chloride crystallisation for any temperature or ΔT applied. To provide this characterisation, in-situ non-invasive

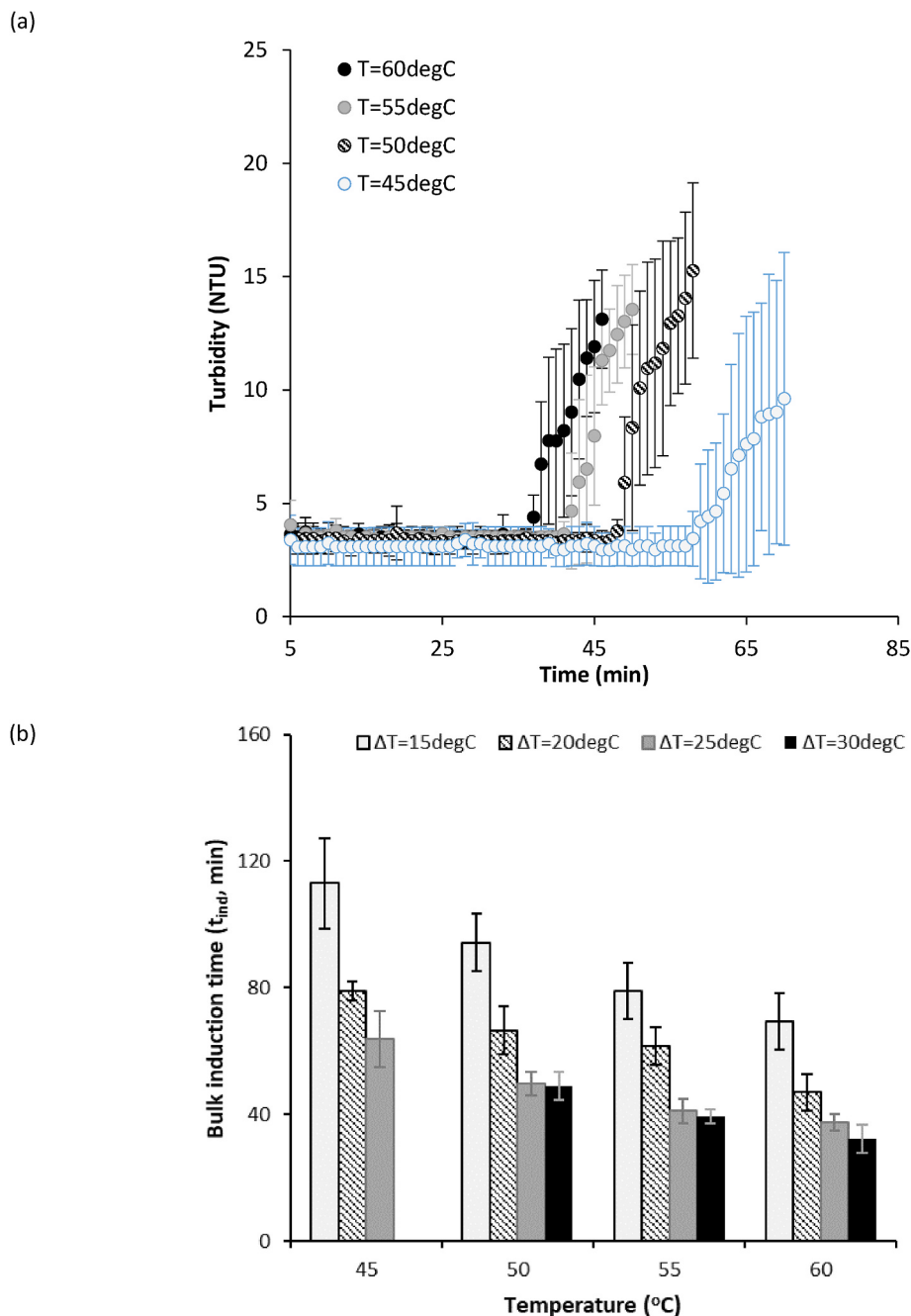


Fig. 3. Induction time is a measure of the metastability of the system: (a) using turbidimetry to determine the time when bulk nucleation begins (illustrative data provided for T 45–60 °C, ΔT 25 °C); and (b) induction time calculated for each experimental condition (T 45–60 °C, ΔT 15–30 °C) which is the difference in time from when the system first produces a stable crystal phase, and the time at which the system exceeded saturation ($C/C^* = 1$). Error bars indicate standard deviation of at least three replicated experiments undertaken at the same conditions.

techniques are used to quantify when scaling and crystallisation within the bulk solution begin. This permits induction time to be estimated for scaling and crystallisation within the bulk solution to enable the independent characterisation of each crystallisation process, elucidation of the preferential primary nucleation pathway, and enhancing understanding of the origin of crystallisation in membrane processes. Through this analytical approach, the supersaturation level can be derived at the point of induction for the bulk and interfacial boundary layer to provide a definitive explanation for which region primarily controls nucleation and crystal growth when temperature or ΔT are used to modify mass and heat transfer processes in MDC. The intended outcome is to establish a unified approach for the characterisation of nucleation in membrane

systems that can be used to provide a holistic description of the nucleation pathway, therefore enabling the mitigation of scaling in favour of advanced control over crystal growth within the bulk solution in membrane processes.

2. Materials and methods

2.1. Membrane distillation crystallisation experimental setup and operation

A direct-contact membrane distillation (DCMD) setup was used (Fig. 1). A 0.95 M sodium chloride (NaCl, 99.5 %, ACROS Organics™,

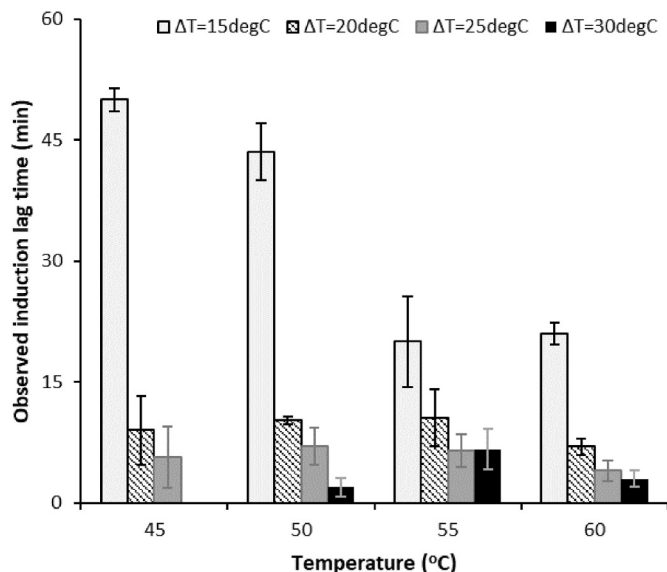


Fig. 4. Lag time observed between the turbidity response and delayed flux response to bulk crystallisation. The precision and accuracy of flux as a surrogate measure of induction improves with an increase in T and ΔT . Error bars indicate standard deviation of at least three replicated experiments.

Fisher Chemicals, Loughborough, UK) feed solution and deionised water ($\approx 15.0 \text{ M}\Omega \text{ cm}$) permeate stream were recirculated counter-currently through the vertically mounted membrane module. The feed Reynolds number (Re) was fixed at 1750. The permeate flow rate was set at 65 % of the feed flow rate. A flat-sheet ePTFE membrane was used which was $50 \mu\text{m}$ thick and possessed a $0.1 \mu\text{m}$ pore size (Cobetter Filtration, Hangzhou, China). The measured water contact angle was 142° . The total surface area was 0.004 m^2 . The feed solution was heated prior to entering the membrane module using an inline heat exchanger (LT ecocool 150, Grant Instruments (Cambridge) Ltd., Shepreth, UK). Fluid temperatures were monitored and recorded using thermocouples ($\pm 0.22^\circ\text{C}$, EI-1034, Electronic Innovations Corporation, Colorado, USA) connected to a data logger (LabJack T7 Pro, LabJack Corporation, Colorado, USA). The feed solution was mixed (300 rpm) with an overhead stirrer (Hei-TORQUE Ultimate 400, Heidolph Instruments, Schwabach, Germany). The permeate stream was cooled in the permeate vessel by passing cold water from the chiller (LT ecocool 150, Grant Instruments Ltd., Shepreth, UK) through the vessel jacket. A precision balance (Cole Parmer Symmetry PT-4202E, Antylia Scientific, Illinois, USA) was used to measure the mass of permeate every minute. Continual permeate conductivity measurements (every minute) (SevenGo™ Pro S7, Mettler-Toledo Ltd, Leicester, UK) were taken to ensure that no salt breakthrough occurred. An inline turbidity probe (InPro 8200/S/ Epoxy/120 turbidity sensor, Mettler-Toledo Ltd, Leicester, UK) was inserted in the feed solution with data recorded every second. The dual optic fibre sensor uses the backscatter technique to provide high resolution detection of induction time enabling reproducible particle detection, and is used extensively for the characterisation of nucleation kinetics [9,23]. A digital microscope (UHM350-11, AmScope, Reigate, UK) was used to provide non-invasive high-resolution imaging of the membrane surface in real time ($1280 \times 720 \text{ p}$). The working distance was $30\text{--}145 \text{ mm}$, which was compatible with the wall thickness and channel depth (22 mm combined) of the polished Perspex cell and enabled a field of view across the full membrane surface. Videos were recorded at 30 frames per second (fps) with observation of crystal growth discriminated to single pixel definition (up to $2.2 \mu\text{m pixel}^{-1}$ dependent on field of view). Due to the extent of supersaturation and the reduction in solution solubility (c^*) instigated by the boundary layer conditions, crystal growth rates (G) for scaling are extremely fast (G exceeding $3 \mu\text{m s}^{-1}$ have been recorded [9]), which means that the crystal is consequently

observable within a few seconds of its formation [24]. The induction time for scaling was recorded at the time the first formed crystal is observable at the membrane surface and is therefore analogous to nucleation detection techniques based on backscatter that are widely deployed for the determination of induction time in solution. The induction time for scaling, and the scaling surface coverage were both subsequently determined through image analysis. Further information on this method can be found in Ref. [9].

2.2. Experimental analysis

To obtain crystal size distributions (CSDs), the crystalliser suspension was vacuum filtered using a $0.45 \mu\text{m}$ nitrocellulose membrane filter (Whatman® NC45, Cytiva, Maidstone, UK) 10 min after the onset of bulk nucleation. The filtered crystals were then allowed to dry in open air at room temperature for at least 48 h before analysis using an optical microscope (CTR 5500 B, Leica Microsystems Ltd, Milton Keynes, UK) in conjunction with a digital camera (SC50 5 MP, Olympus, Southend-on-Sea, UK). A sample of at least 1000 crystals was analysed using Olympus Stream Image Analysis Software (Olympus, Southend-on-Sea, UK) to obtain the CSDs. The crystals deposited on the membrane surface were also filtered at the end of each experiment. Residence time for the crystals was fixed by waiting 10 min after bulk nucleation prior to sampling. Crystal and membrane samples were characterised using scanning electron microscopy (SEM) (VEGA 4, Tescan Orsay Holding, Czech Republic). Samples were coated with a 10 nm coating of gold by physical vapour deposition (acceleration voltage, 20 keV ; beam current, 300 pA ; working distance, 10 mm).

2.3. Data analysis

For each experiment, the permeate flux was calculated based on the permeate mass accumulated over time:

$$J_p = \frac{\Delta m}{A_m \Delta t} \quad (1)$$

where J_p ($\text{kg m}^{-2} \text{ s}^{-1}$) is the permeate flux, A_m (m^2) is the membrane surface area, and Δm (kg) and Δt (s) are the changes in permeate mass and time, respectively. A 5-min average of the permeate flux was used in calculations to account for experimental error. It was assumed that only water vapour passed through the membrane module. This assumption was validated by the permeate conductivity measurements which showed no evidence of salt breakthrough. Hence, the change in feed concentration could be directly calculated based on the mass of permeate vapour recovered.

The metastable zone width (MSZW) can be described using either the concentration (ΔC_{max} , kg m^{-3}) or supersaturation (S_{max}) at induction as follows:

$$\Delta C_{\text{max}} = C_{\text{max}} - C_{\text{sat}} \quad (2)$$

$$S_{\text{max}} = \frac{C_{\text{max}}}{C_{\text{sat}}} \quad (3)$$

where C_{max} (kg m^{-3}) and C_{sat} (kg m^{-3}) are the actual (maximum) and saturation concentrations at induction, respectively. The quantity ΔC_{max} represents the width or extent of the metastable zone width at nucleation, whereas S_{max} is a dimensionless parameter in which the solute concentration at nucleation is normalised by the solute concentration representing the solubility limit in solution for the specific conditions studied. The bulk induction time was determined based on the inflection point of the turbidity-time trends and the scaling induction time was obtained by analysis of online digital microscope images. The temperature and concentration polarisation coefficients (TPC and CPC respectively) were calculated and applied to obtain the MSZWs within the boundary layer at the membrane interface (interfacial supersaturation) [25]:

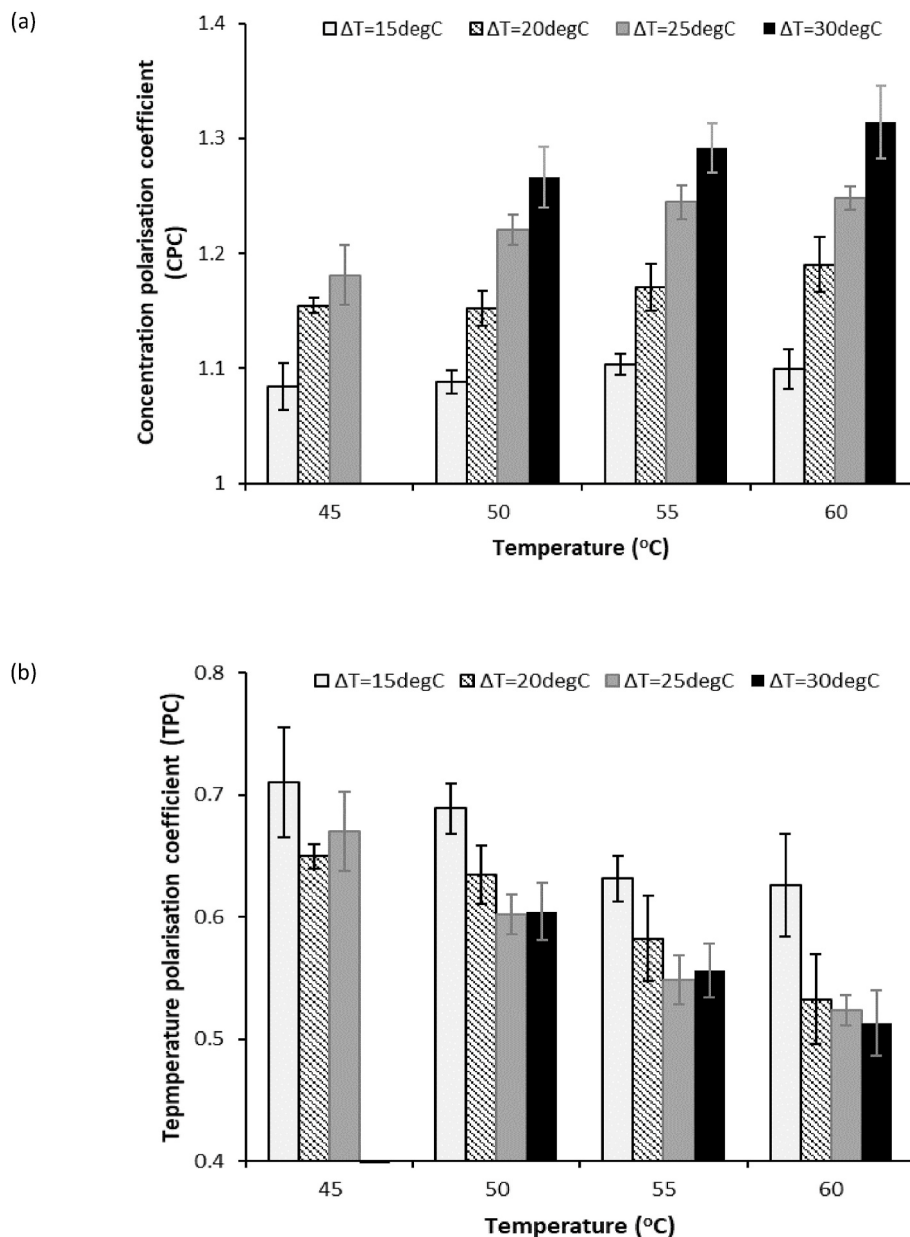


Fig. 5. Characterisation of concentration and temperature polarisation coefficients (CPC, TPC) which determine the interfacial saturation level at the onset of bulk nucleation: (a) CPC; and (b) TPC. Conditions: T 45–60 °C, ΔT 15–30 °C. Error bars indicate standard deviation of at least three replicates.

$$\Delta G_{int} = G_{int} - C_{sat}(T_{int}) \quad (4)$$

$$S_{int} = \frac{C_{int}}{C_{sat}(T_{int})} \quad (5)$$

where the subscript *int* refers to the interface and $C_{sat}(T_{int})$ is the saturation concentration at the interfacial temperature (T_{int} , K). The interfacial concentration (C_{int} , kg m⁻³) is determined from the bulk concentration (C_b , kg m⁻³) as follows:

$$C_{int} = C_b(CPC) = C_b \exp\left(\frac{J_p}{\rho K}\right) \quad (6)$$

where ρ (kg m^{-3}) is the solution density and K (m s^{-1}) is the mass transfer coefficient based on the L  v  que solution for laminar flow:

$$K = \frac{1.62D}{d_h} \left(\frac{V d_h^2}{DL} \right)^{\frac{1}{3}} \quad (7)$$

D ($\text{m}^2 \text{s}^{-1}$) is the molecular diffusivity or diffusion coefficient, d_h (m) is the hydraulic diameter, V (m s^{-1}) is the feed solution velocity, and L (m) is the length of the membrane surface. The TPC is the ratio between the interfacial and bulk temperature differences [26]:

$$TPC = \frac{\Delta T_{int}}{\Delta T_b} = \frac{T_{int} - T_{int,p}}{T_{b,f} - T_{b,p}} \quad (8)$$

where subscripts b , f and p refer to the bulk, feed and permeate, respectively. A steady-state energy balance of the heat transfer from the bulk feed to the bulk permeate solution yields the following equation for the interfacial feed temperature which must be solved iteratively using the subsequent equations:

$$T_{int} = \frac{\frac{k_m}{\delta_m} \left(T_p + \left(\frac{h_f}{h_p} \right) T_f + h_f T_f - J_p \Delta H_v \right)}{\frac{k_m}{\delta_m} + h_f + \frac{k_m}{\delta_m} \bullet \frac{h_f}{h_a}} \quad (9)$$

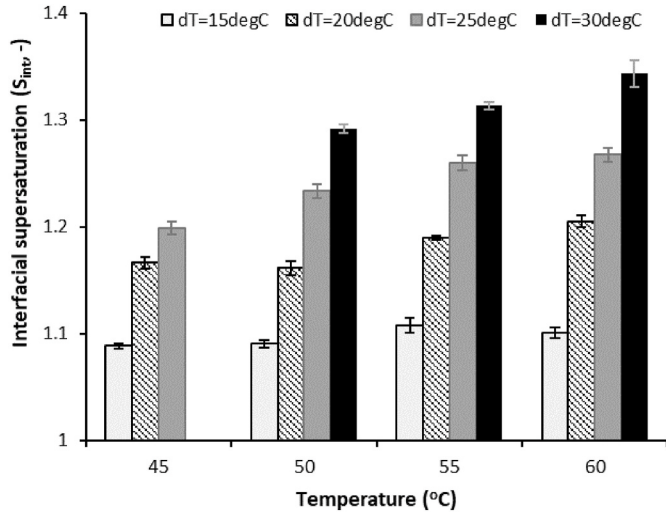


Fig. 6. Comparison of supersaturation conditions within the interfacial region at the onset of bulk nucleation. Conditions: T 45–60 °C; ΔT 15–30 °C. Error bars indicate standard deviation of at least three replicates.

$$T_{int,p} = \frac{\frac{k_m}{\delta_m} \left(T_f + \left(\frac{h_p}{h_f} \right) T_p + h_p T_p + J_p \Delta H_v \right)}{\frac{k_m}{\delta_m} + h_p + \frac{k_m}{\delta_m} \cdot \frac{h_p}{h_f}} \quad (10)$$

where δ_m (m) is the thickness of the membrane, ΔH_v (J kg⁻¹) is the latent heat of vaporisation and k_m (W m⁻¹ K⁻¹) is the thermal conductivity of the membrane which is calculated using the isostress model [27]:

$$k_m = \left(\frac{\varepsilon}{k_{gas}} + \frac{1-\varepsilon}{k_{solid}} \right)^{-1} \quad (11)$$

where ε is the membrane porosity. The thermal conductivities of the water vapour/air gas mixture (k_{gas} , W m⁻¹ K⁻¹) and solid polymer (k_{solid} , W m⁻¹ K⁻¹) were calculated using the following correlations [27]:

$$k_{gas} = 1.5 \times 10^{-3} \sqrt{T} \quad (12)$$

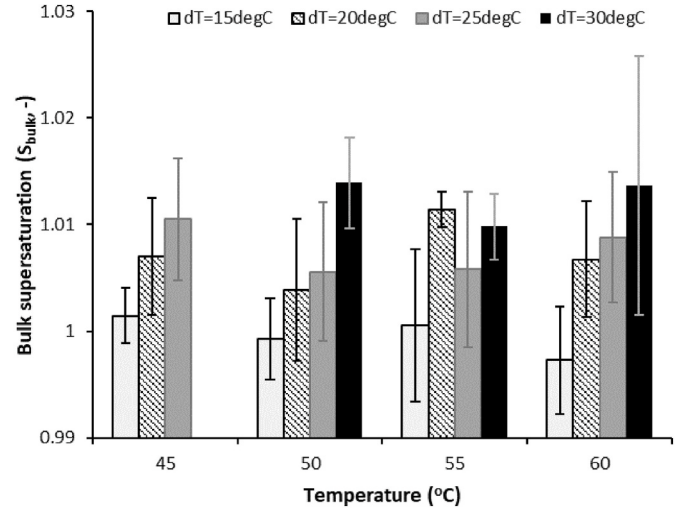


Fig. 8. Comparison of supersaturation levels within the bulk solution at the onset of bulk nucleation. Conditions: T 45–60 °C; ΔT 15–30 °C. Error bars indicate standard deviation of at least three replicates.

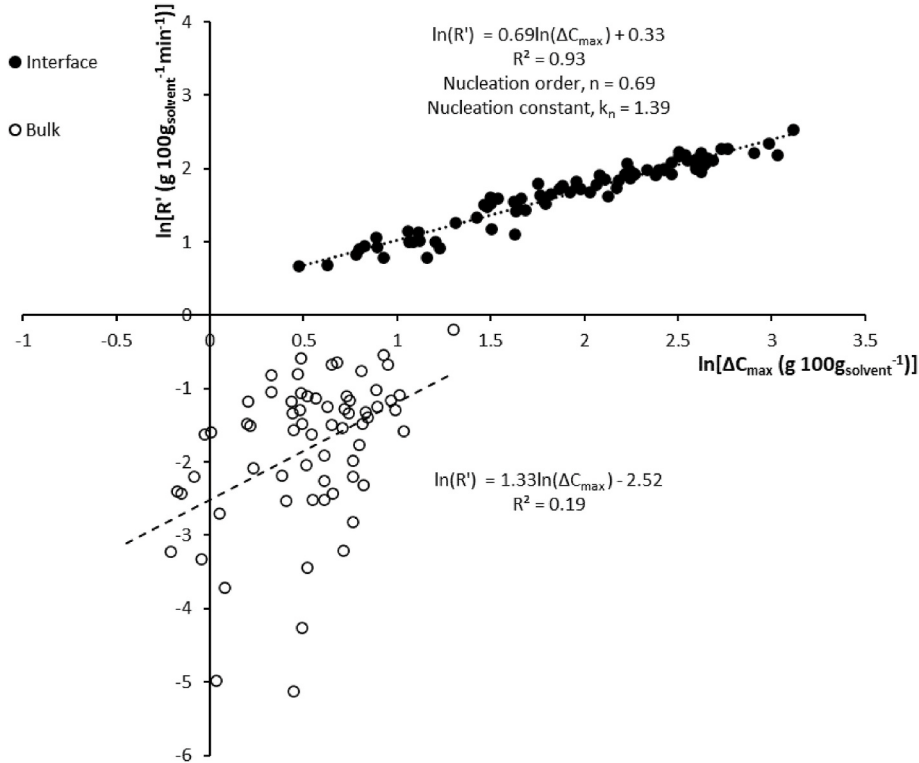


Fig. 7. Comparing the relationship between metastable zone width (MSZW, ΔC_{max}) and supersaturation rate (R') at induction based on interfacial and bulk solution concentrations from the complete data set (T 45–60 °C; ΔT 15–30 °C). Nyvlt's [22] modified method (linear trend for each discrete dataset) provides a description of the nucleation kinetics. The stronger data fit to interfacial concentration suggests that crystals found in the bulk solution are primarily formed near the membrane interface.

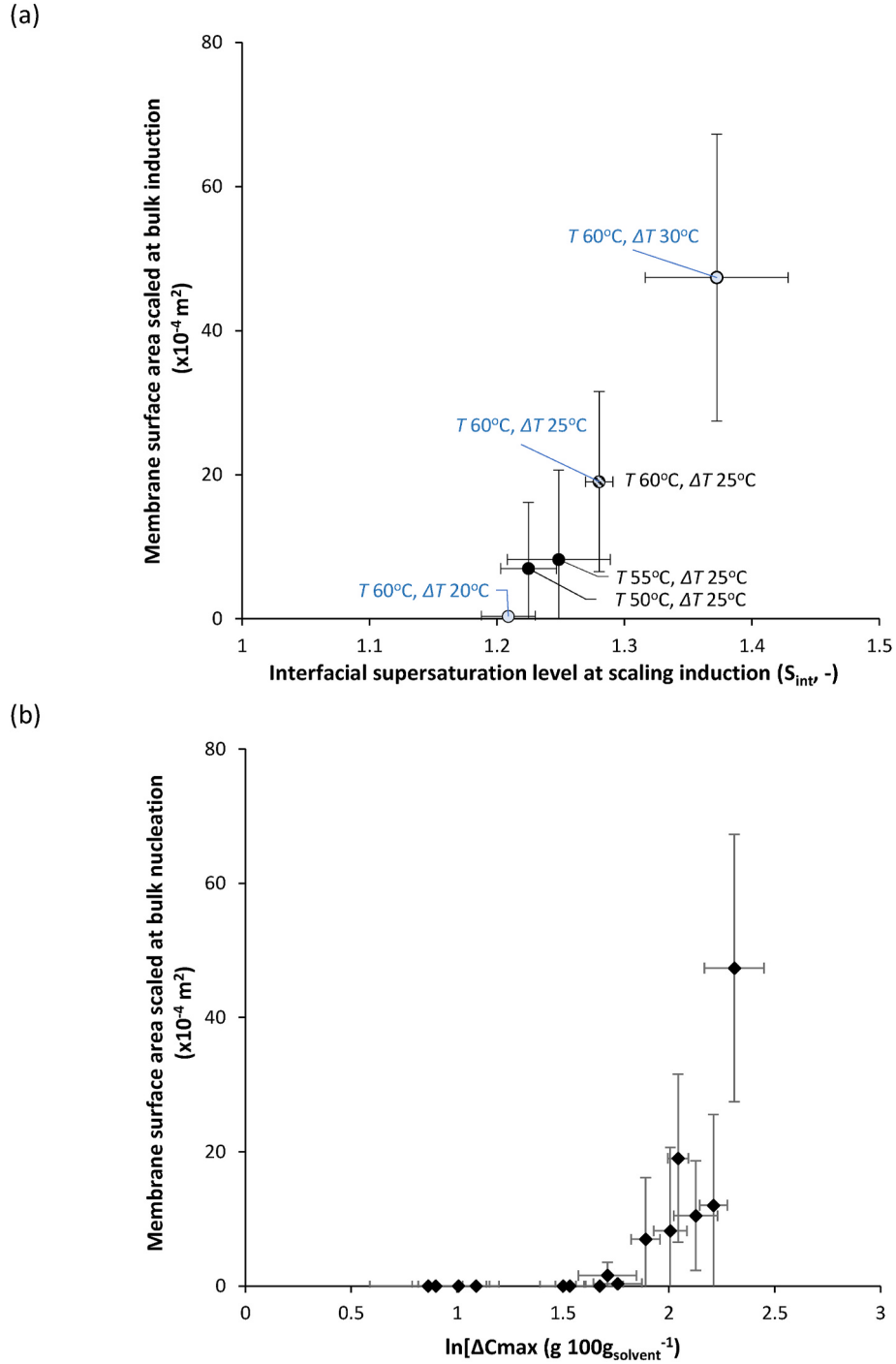


Fig. 9. Relating interfacial supersaturation level (S_{int}) to the extent of scaling up to the onset of bulk nucleation (T 50–60 °C, ΔT 20–30 °C): (a) Illustrating the discrete roles of T and ΔT on scale formation; and (b) Complete dataset demonstrating transition from conditions where no scaling exists to where scaling proceeds (T 45–60 °C, ΔT 15–30 °C). Error bars indicate standard deviation of at least three replicates.

$$k_{solid} = 4.86 \times 10^{-4} T + 0.253 \quad (13)$$

h_f ($\text{W m}^{-2} \text{K}^{-1}$) and h_p ($\text{W m}^{-2} \text{K}^{-1}$) are the feed and permeate heat transfer coefficients, respectively:

$$h_f = \frac{Nuk_f}{d_h} \quad (14)$$

$$h_p = \frac{Nuk_p}{d_h} \quad (15)$$

where k_f ($\text{W m}^{-1} \text{K}^{-1}$) and k_p ($\text{W m}^{-1} \text{K}^{-1}$) are the feed and permeate conductivities, respectively. The Nusselt number, Nu , is dimensionless, and is calculated with other dimensionless parameters including the Reynolds number (Re) and Prandtl (Pr) number [26]:

$$Nu = 0.023 Re^{0.8} Pr^{\frac{1}{3}} \quad (16)$$

$$Re = \frac{\rho V d_h}{\mu} \quad (17)$$

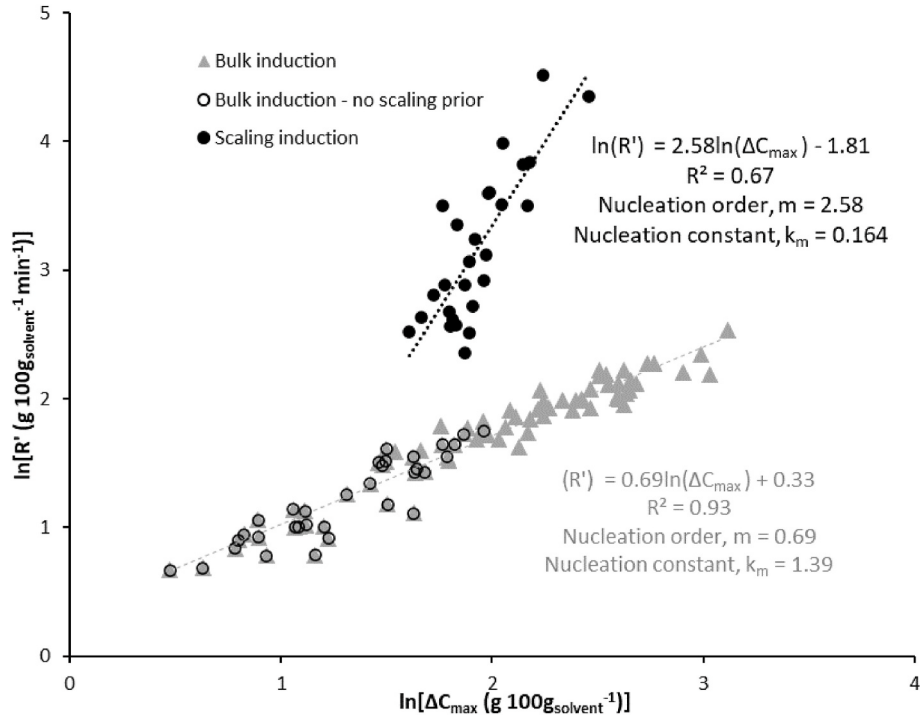


Fig. 10. Establishing the relationship between metastable zone width (MSZW, ΔC_{max}) and supersaturation rate (R') at induction based on interfacial concentrations for: (i) bulk induction (distinguished between data where scaling was also present or absent); and (ii) scaling induction (black closed circles). Complete dataset (T 45–60 °C, ΔT 15–30 °C) is shown for bulk nucleation which occurred irrespective of scaling.

$$Pr = \frac{c_p \mu}{k} \quad (18)$$

where μ (Pa s) is the dynamic viscosity, c_p ($J kg^{-1} K^{-1}$) is the specific heat capacity, and k ($W m^{-1} K^{-1}$) is the thermal conductivity of the respective solutions. The solution properties were determined using Aspen Plus, applying the Elec-NRTL thermodynamic model which is an appropriate model for highly-concentrated electrolyte solutions [15].

According to Nývlt [22], the operating window of a crystallisation process can be defined by applying MSZW measurements to characterise the nucleation kinetics. Nývlt's [22] method was based on classical nucleation theory (CNT) which assumes an empirical power law relationship between the nucleation rate and the MSZW:

$$B_m = k_m \Delta C_{max}^m \quad (19)$$

where B_m ($kg m^{-3} s^{-1}$) is the nucleation rate (mass basis), and k_m ($kg m^{-3} s^{-1}$) and m are the nucleation rate constant and apparent nucleation order, respectively. It is assumed that at the point of induction (onset of nucleation or vicinity of metastability), the rate of supersaturation is equal to the nucleation rate [22]. Therefore,

$$R' = k_m \Delta C_{max}^m \quad (20)$$

where R' ($kg m^{-3} s^{-1}$) is the supersaturation rate in the vicinity of metastability. The validity of this assumption is based on assuming that the surface area of the initial crystals is still very small, and the nucleation rate is therefore significantly higher than the growth rate. To account for experimental fluctuations, the supersaturation rate was taken as the average rate from the start of the experiment to the point of induction:

$$R' = \frac{\Delta C_{max} - \Delta C_0}{\Delta t_{nucl}} \quad (21)$$

where ΔC_0 is the starting saturation level and Δt_{nucl} is the time required for nucleation to take place from the start of the experiment. Linearisation of Eq. (21) yields:

$$\ln(R') = \ln(k_m) + m[\ln(\Delta C_{max})] \quad (22)$$

Linear regression of the plot of $\ln(\Delta C_{max})$ versus $\ln R'$ will then yield m as the gradient of the line of best-fit. k_m can be obtained by calculating the exponential function of the y-intercept.

The crystal growth rate, G , was calculated based on the growth rate equation for mixed suspension mixed product removal (MSMPR) crystallisers [28]:

$$G = \frac{6L_{50}^4 \alpha B_n}{\varphi} \quad (23)$$

where L_{50} (m) and α are the median size and shape factor, respectively. B_n ($m^{-3} s^{-1}$) is the nucleation rate (number basis, assumed based on R') and φ is the volumetric holdup of crystals in suspension:

$$\varphi = \frac{V_c}{V_{susp}} = \frac{V_c}{V_c + V_{sol}} \quad (24)$$

where, V_c (m^3), V_{susp} (m^3) and V_{sol} (m^3) are the crystal, suspension and solution volumes, respectively.

The primary nucleation mechanism may be dependent on the presence of a foreign surface to reduce the effective interfacial energy, which reduces the activation energy required for nucleation. Hence, the lower the interfacial energy, the greater the likelihood that heterogeneous nucleation will predominate over homogeneous nucleation [2,29,30]. Classical nucleation theory assumes an inversely proportional relationship between nucleation rate and induction time, where the relationship between induction time (t_{ind} , s) and supersaturation level (S) at the onset of nucleation is described by Ref. [30]:

$$\ln(t_{ind}) = K + \frac{16\pi\gamma^3 v^2}{3(k_B T)^2 \ln^2 S} \quad (25)$$

where K is a constant, γ ($J m^{-2}$) is the interfacial energy, v (m^3) is the volume of the solute molecule, k_B is the Boltzmann constant, and T (K) is the nucleation temperature. A plot of $\ln(t_{ind})$ against $\ln^{-2} S$ at constant

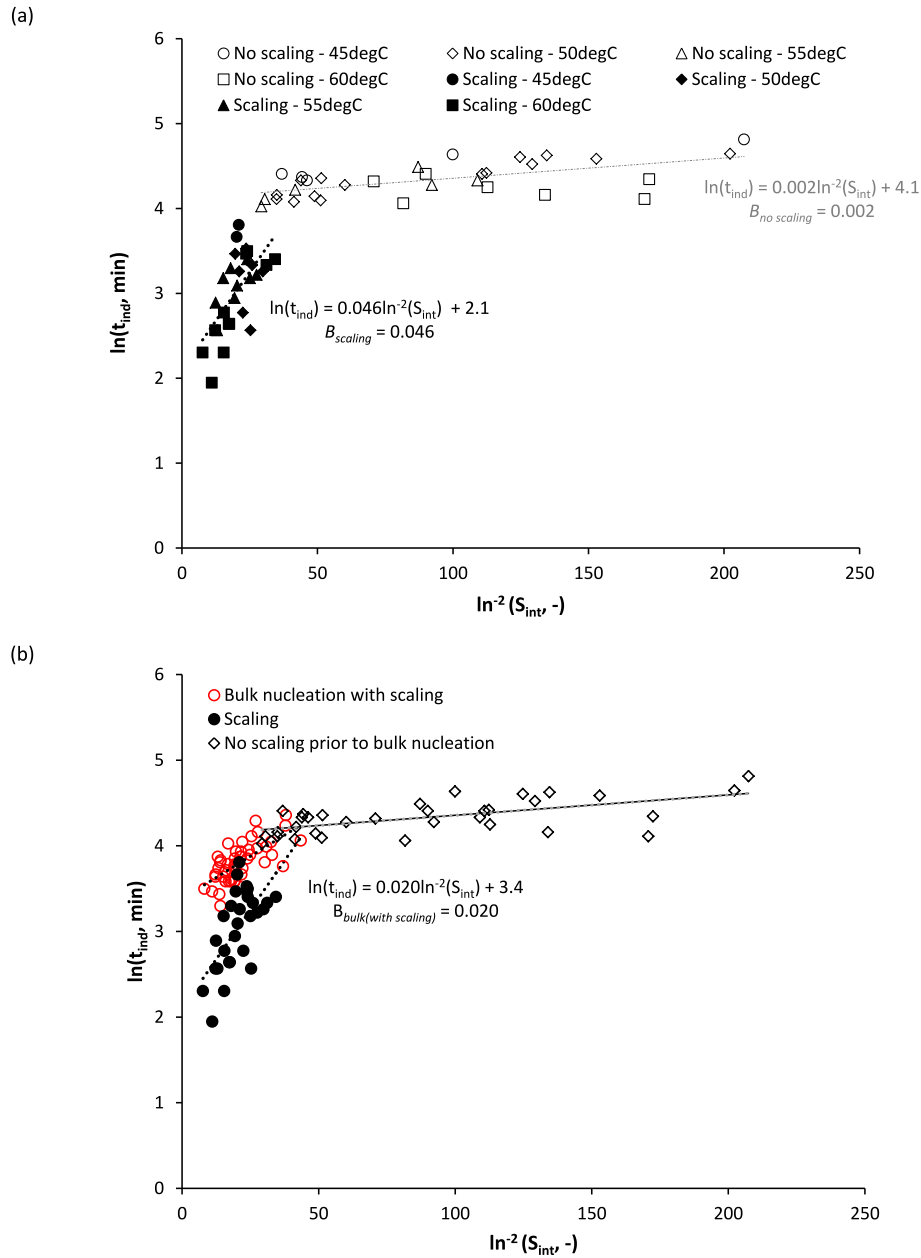


Fig. 11. (a) Relating induction time to the interfacial supersaturation level (T 45–60 °C, ΔT 15–30 °C) for data where scaling preceded bulk nucleation (closed symbols), or where bulk nucleation occurred first in the system (open symbols, i.e. where scaling was not observed). Classical nucleation theory describes two regions: (i) a region of elevated supersaturation characterised by a steeper gradient (B) which favours homogeneous primary nucleation; and (ii) a region of low supersaturation which favours heterogeneous primary nucleation [29,30]; and (b) characterisation of bulk crystallisation following scaling.

temperature yields a linear trend with gradient (B):

$$B = \frac{16\pi\gamma^3 v^2}{3(k_B T)^2} \quad (26)$$

Hence, steeper gradients indicate higher interfacial energies and a tendency towards homogeneous nucleation. Conversely, a lower gradient evidences a lower interfacial energy and enhanced probability of heterogeneous nucleation [29,30].

3. Results and discussion

3.1. Characterisation of flux and induction time when modified by temperature and ΔT

Permeate flux was characterised across a range of feed temperatures

(45–60 °C) and ΔT (15–30 °C). At a fixed ΔT of 25 °C, an increase in T from 45 to 60 °C raised the permeate flux from 20.7 to 30.7 kg m⁻² h⁻¹ at induction (Fig. 2a). The increase in permeate flux with T was due to the exponential dependence of vapour-pressure difference on temperature in accordance with the Antoine equation [16]. For each feed temperature (45–60 °C), an increase in ΔT from 15 to 30 °C resulted in a higher permeate flux (Fig. 2b). This is due to the temperature difference which enhanced the vapour pressure difference between the feed and permeate solutions, increasing the driving force for mass transfer [31].

Induction time was characterised in the bulk solution by turbidimetry (Fig. 3a). Induction time represents a measure of the metastability of a system, as it is defined as the time taken to produce a crystal phase once saturation has been achieved ($t_{ind} = t_{crys} - t_{c/e=1}$). An induction time was determined for each set of conditions tested; this illustrates that a crystal phase was produced in the bulk solution for each T and ΔT studied. An increase in feed solution temperature, or ΔT , shortened

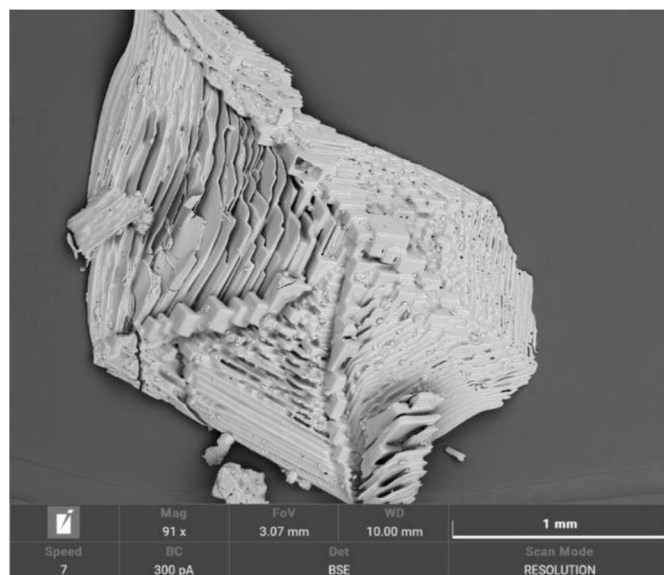


Fig. 12. Scanning electron microscopy (SEM) image of scaling illustrating dendritic hopper morphology. Conditions: T 55°C, ΔT 25°C.

induction time (Fig. 3b). The shortest induction time was recorded for the highest temperature and ΔT used. To illustrate, an induction time of 113 min was recorded for T and ΔT of 45 and 15 °C respectively, whereas induction time shortened to 32 min when T and ΔT were 60 and 30 °C respectively. The measured induction times were compared to those characterised using the conventional approach of a rapid flux decline as a surrogate measure of induction (Fig. 4). This analysis consistently identified a lag time between the occurrence of crystallisation in the bulk solution, and the onset of a flux decline. The lag time generally increased with a reduction in T and ΔT . The longest lag time of 50 min was observed with T and ΔT of 45 and 15 °C respectively, which represents the lowest driving force employed. The sensitivity of flux decline as a surrogate measure of induction is therefore further compromised at lower permeate fluxes. Importantly, this data evidences that primary nucleation is not principally responsible for the flux decline in MDC, which contradicts previous suggestions in the literature. This confirms that a stable crystal phase can be produced within the bulk solution without necessarily incurring a diminution in flux.

3.2. Determination of supersaturation at the onset of bulk crystallisation

Concentration and temperature polarisation are adjusted at the membrane interface by changes to T and ΔT . The concentration polarisation coefficient (CPC) increased with T and ΔT due to the rise in water vapour flux (Fig. 5a). Consequently, the interfacial (boundary layer) solute concentration increased with T and ΔT , which can then increase the interfacial supersaturation level. However, an increase in T and ΔT also decreased the temperature polarisation coefficient (TPC), resulting in lower interfacial temperatures (Fig. 5b). Sodium chloride possesses a slight inverse solubility-temperature dependency. Hence, a reduction in interfacial temperature will lower the solubility constant, which enhances the interfacial supersaturation level (S_{int}) at induction (Fig. 6). For example, at a constant T 60 °C, the S_{int} recorded at induction for the bulk crystal phase, increased from 1.10 to 1.34 when ΔT rose from 15 to 30 °C. Higher T and ΔT therefore increased the driving force for nucleation within the boundary layer.

In order to relate the role of T and ΔT to the mechanism of nucleation in MDC, the approach of Nývlt [22] was modified to characterise the supersaturation rate and metastable zone width within the bulk and interfacial regions for each of the T and ΔT conditions (Fig. 7). According to classical nucleation theory (CNT), the dependence of

nucleation rate on the maximum supersaturation level is exponential. Within this analysis, supersaturation rate is a direct analogy to nucleation rate. Hence, by applying the method adapted from Nývlt [22], a linear relationship should be observed between the natural logarithms of the supersaturation rate and the MSZW. A linear relationship (r^2 , 0.93) was obtained for interfacial conditions based on the supersaturation achieved at the point of induction for the bulk crystal phase across the complete range of conditions (T 45–60 °C; ΔT 15–30 °C). The MSZW increased with T and ΔT due to higher permeate fluxes which modified the interfacial conditions. The broader MSZW is attributed to the faster supersaturation rates set by the higher permeate flux. For these conditions, there is not sufficient time for the system to adjust to each supersaturation level, instigating a non-equilibrium condition where the perceived energy barrier is higher than the actual energy barrier of the solution and the likelihood of nucleation is reduced. This lag between the perceived and actual states of solution results in a wider MSZW [32, 33]. The gradient of the curve represents the solute-solvent interactions between sodium chloride and water, where the low interfacial energy of NaCl requires a low level of supersaturation to initiate nucleation, resulting in relatively small nucleation rates. Consequently, this analysis confirms that the primary nucleation kinetics of the bulk crystal phase are determined by the interfacial supersaturation set at the membrane and can be collectively represented by the analytical approach proposed.

There was no statistically significant relationship demonstrated between the supersaturation level set in the bulk conditions (ΔC_{max} , open circles), and the supersaturation rate (R'). To further investigate the role of the bulk solution, the absolute value of the bulk supersaturation level (S_{bulk}) was characterised at the point the bulk crystal phase was identified by turbidimetry (induction) (Fig. 8). For each T and ΔT studied, supersaturation was consistently recorded at a S value of ~ 1 . This is equal to the solubility limit of solution (i.e. saturation, or $c/c^* = 1$). For crystallisation to occur, the chemical potential of NaCl in solution must exceed that of the crystal phase [14]. While the interfacial supersaturation exceeded this threshold, the newly 'birthed' nuclei formed within this region will dissolve in the bulk solution unless $S > 1$, as it is only once this threshold is exceeded that the system has sufficient chemical potential to sustain a thermodynamically stable 'critical' nucleus. Therefore, while the nucleation kinetics are defined by supersaturation within the interfacial boundary layer, a crystal phase cannot form in the bulk solution until saturation ($c/c^* \sim 1$) is met.

3.3. Establishing a kinetic description of scaling

The role of T and ΔT in the formation of scaling was undertaken with digital microscopy, where the extent of scaling that occurred up to the point of bulk nucleation could be quantified (Fig. 9). Raising feed temperature (ΔT fixed at 25 °C) resulted in a modest increase in the extent of scaling observed and was coincident with an increased interfacial supersaturation level at induction (of the bulk crystal phase). According to CNT, an increase in solution temperature should decrease the MSZW due to the increased likelihood of molecular attachments which reduces the activation energy requirement for nucleation [6,14]. However, in MD, an increase in feed temperature also increases permeate flux, which modifies the supersaturation rate subsequently broadening the MSZW. Therefore, temperature *indirectly* increased the extent of scaling through kinetically modifying S_{int} , which has implications for both the nucleation rate and growth rate of scaling. An increase in ΔT (T fixed at 60 °C) provided a greater increase in scaling due to the larger transition in mass and heat transfer processes within the boundary layer. The extent of scaling was subsequently compared for each T and ΔT studied to characterise the transition in scaling based on the relative supersaturation driving force (Fig. 9b). Below a metastable zone width ($\ln \Delta C_{max}$) of around 1.9, no scaling was observed prior to formation of the bulk crystal phase (see also Fig. 10, open circles). Above this value, scaling was measurable prior to bulk nucleation, where the extent of scaling was

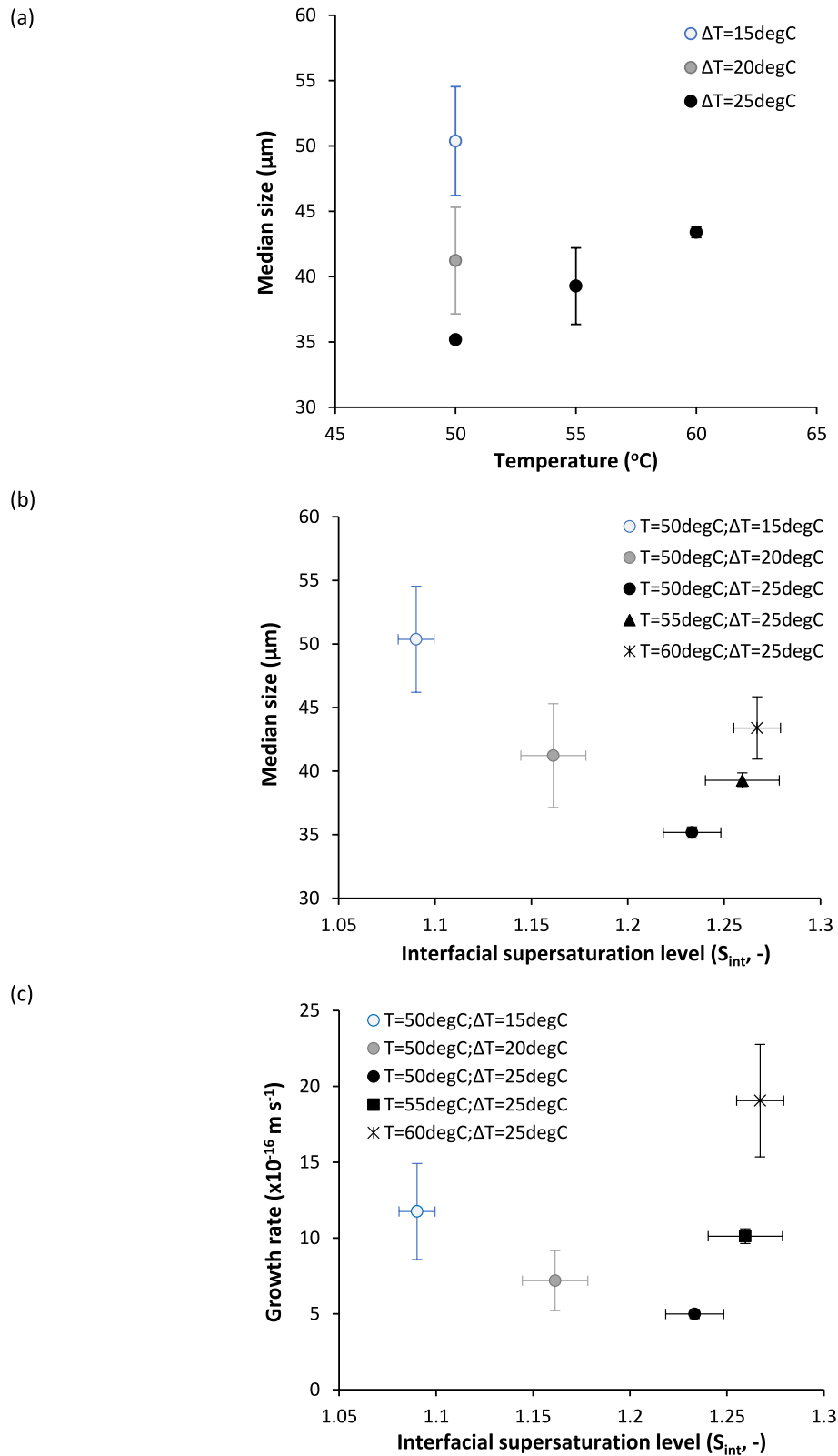


Fig. 13. Relating interfacial conditions to conditions for crystal growth (T 50–60 $^{\circ}\text{C}$; ΔT 15–30 $^{\circ}\text{C}$): (a) Median crystal size; (b) Median crystal size related to interfacial supersaturation; and, (c) crystal growth rate. Error bars indicate standard deviation of at least three replicates.

dependent on the supersaturation driving force in the boundary layer. The supersaturation and supersaturation rate were also measured at the induction time for scaling to better understand the nucleation kinetics (Fig. 10). The supersaturation rate (R') recorded for scaling was considerably higher than for the bulk crystal phase, which is due to the

higher fluxes at scaling induction, leading to greater concentration polarisation and solute concentration within the boundary layer. Consequently, the nucleation rate for scaling at induction exceeds the nucleation rate for the bulk crystal phase. This is exemplified by the nucleation order (m) derived for bulk nucleation and scaling nucleation

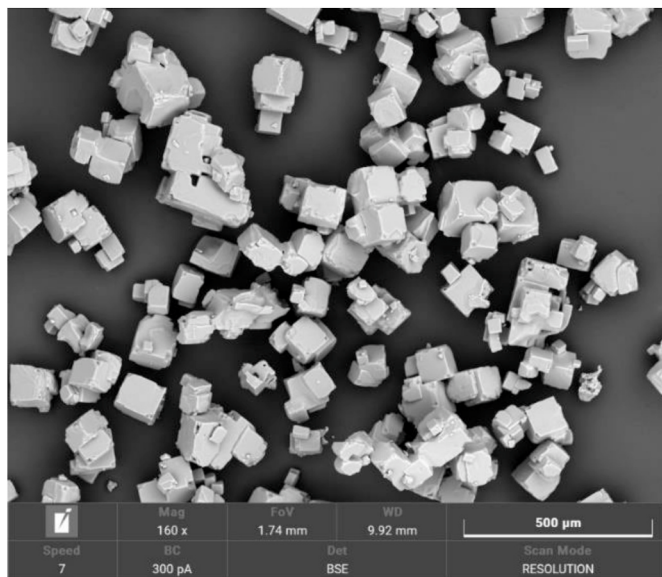


Fig. 14. Scanning electron microscopy (SEM) image of bulk crystals, evidencing cubic morphology. The crystals presented here are formed in the bulk solution at conditions (T 55°C, ΔT 25°C) characterised by a homogeneous primary nucleation mechanism, where scaling also occurs.

which were 0.69 and 2.58 respectively. Both values indicate strong diffusive interactions between sodium chloride and water which promote the aggregation and growth of nuclei; the higher order for scale emphasising how the elevated interfacial concentration reduces the distance between the solute molecules to favour cluster formation.

The primary nucleation mechanism that governs how scaling and the bulk crystal phase are formed, can be determined through investigating the relationship between induction time and supersaturation (Eq. (25)). Induction times for each set of conditions studied (T and ΔT) are initially

presented based on where primary nucleation first occurred in the system, i.e. t_{ind} represents the metastable period either up to when scaling first began to form (black symbols), or, when scaling did not occur, t_{ind} represents the metastable period up to when the bulk crystal phase was first identified (open symbols) (Fig. 11a). Two discrete domains were identified: (i) a region of low supersaturation characterised by longer induction times in which bulk crystals were first formed without the presence of scaling; and (ii) a region of high supersaturation, where t_{ind} exhibited a stronger dependence upon supersaturation which describes conditions in which scaling occurred. The value of the slope (B) represents the energy barrier for nucleation [20]. The shallow gradient (B , 0.002) reported for the bulk crystal phase is indicative of favouring heterogeneous primary nucleation, whereas the steep slope representing the kinetics of scaling, is indicative of homogeneous primary nucleation (B , 0.046). It has previously been assumed that the bulk crystal phase is first formed on the membrane by a heterogeneous primary nucleation mechanism where it grows to a critical size (based on a force balance), above which the applied shear stress is presumed sufficient to overcome the attachment forces to enable its backtransport to the bulk solution [8]. However, in this study, it is evident that a crystal phase can be produced without first forming crystals at the membrane surface. The transition to conditions favouring scaling mitigation is therefore denoted by a threshold supersaturation value at the intersection between homogeneous and heterogeneous primary nucleation mechanisms. The bulk crystal phase that is formed when T and ΔT favour scale formation, was also characterised by a homogeneous primary nucleation mechanism, with t_{ind} exhibiting less dependency on supersaturation compared to scaling (B , 0.020; Fig. 11b). For conditions favouring homogeneous crystallisation, t_{ind} is inversely proportional to nucleation rate. This is illustrated by the higher R' recorded for scaling, than for the bulk crystal phase (Fig. 10). As the MSZW reduced toward the threshold supersaturation value that marks the transition between heterogeneous nucleation mechanisms, the nucleation rate (R') for scaling also began to converge with the values established for the bulk crystal phase. This suggests the origin for the heteronuclei or embryos that form scaling and

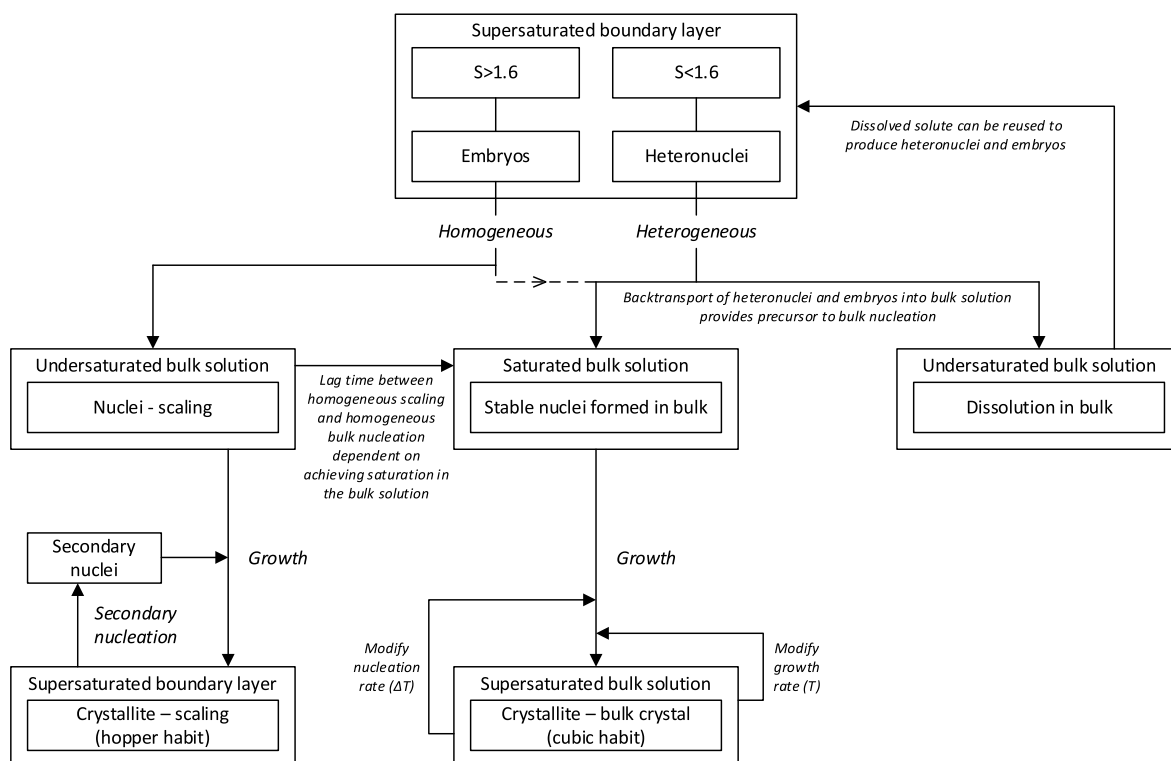


Fig. 15. Mechanism proposed for kinetically controlled nucleation and crystal growth in membrane systems.

the bulk crystal phase may be shared, but that scaling is formed homogeneously due to solute entrapment within the pores and crevasses of the membrane, where exposure to a supersaturation level in excess of this critical supersaturation threshold enables the establishment of a thermodynamically stable crystal phase. Scaling can form in advance of the bulk crystal phase due to its consistent exposure to a supersaturated state that fosters exposure to extremely high nucleation rates, whereas the establishment of the bulk crystal phase requires the bulk solution to achieve saturation ($c/c^* \sim 1$) to enable the thermodynamically stable crystal phase to form, which institutes a time lag and as such, due to temporal modifications of mass and heat transfer processes in the boundary layer, the interfacial conditions at which the bulk crystal phase is produced are distinct from those of scaling.

In previous research on porous media, nucleation of NaCl crystals was also only observed once a critical supersaturation threshold was achieved [24]. The supersaturation threshold identified is equivalent to the supersaturation threshold in this study that marks the transition from a heterogeneous to a homogeneous nucleation mechanism. This threshold was explained as the intersection between extremely small (below unity) and very high nucleation rates, consistent with classic nucleation theory. At this threshold, the high supersaturation level instigated rapid growth of ‘hopper crystals’ which are formed through secondary nucleation occurring at the edges of the primary nuclei, due to faster growth rates at the crystal edges versus the crystal faces. This was illustrated in this study through formation of long thin sheets, and well-aligned ‘branches’ or ‘chain-like’ cubic sectors growing outwards from the primary central cubic crystal (Fig. 12). This is indicative of a two-dimensional nucleation growth mechanism (birth and spread model) where high supersaturation levels are a prerequisite for stability of the adatoms that form on a flat surface [24]. The rapid decrease in local supersaturation during growth consequently favours the formation of only single large skeletal crystals (several thousand microns in diameter). The nucleation rate depends so steeply on the supersaturation level that all other parameters (for example, changes to T or ΔT) are irrelevant, and a critical supersaturation threshold can be identified from this study, below which scaling can be ‘switched-off’ leading to production of only crystals in the bulk solution.

3.4. Control of nucleation, growth and morphology of the bulk crystal phase

Analysis of CSDs indicated that at a fixed temperature (T 50 °C), an increase in ΔT from 15 to 25 °C, decreased median size of the bulk crystals from 50.4 to 35.2 μm (Fig. 13a). This can be explained by the higher supersaturation rate, which raised supersaturation level at induction (Fig. 13b). Supersaturation provides the driving force for nucleation, where higher nucleation rates tend to inhibit crystal growth as there are fewer ions available for growth, resulting in smaller crystal sizes (Fig. 13c) [15]. When sustaining a constant ΔT (25 °C), an increase in T from 50 to 60 °C raised the median crystal size from 35.2 to 43.4 μm . While the interfacial supersaturation increased with T , an increase in T also enhances the kinetics for diffusion-controlled growth which favours a larger median crystal size [34]. The bulk crystal phase comprised of cubic morphology (Fig. 14, T 55 °C, ΔT 25 °C) which is the characteristic crystal habit for NaCl. This is reflective of growth within less supersaturated conditions, providing more time for the absorption and diffusion of solute molecules at the centre of faces to form flat surfaces [24]. The nucleation order (m , Fig. 7) demonstrates that it is possible to estimate nucleation rate for all T and ΔT studied. As such, setting T and ΔT can deliver supersaturation to a set point, where adjustments to nucleation rate (ΔT) and crystal growth (T) can be made to control final product specification. While all feed temperatures studied can be used (45–60 °C), ΔT must be limited to between 15 and 20 °C (dependent upon T) to favour heterogeneous primary nucleation and therefore suppress scaling (Fig. 15).

4. Conclusions

This study has used non-invasive techniques for the direct determination of induction time, enabling differentiation between nucleation mechanisms occurring on the membrane surface and those occurring in the bulk solution, to provide a unified understanding of crystallisation within membrane systems. Whereas the literature has previously supposed that crystallisation occurs in a sequential process where scaling commences followed by detachment via shear-based processes, this study demonstrates two discrete nucleation pathways, where the crystal phase can be formed in the bulk solution in the absence of scaling. For this condition, the crystal phase in the bulk solution is formed via a heterogeneous primary nucleation mechanism. The preferential primary nucleation mechanisms for scale and bulk crystal formation are therefore contrary to those typically perceived in the literature, but the mechanistic explanation is consistent to previous literature observations where scaling is regarded as more tenacious in conditions of higher heat and mass transfer and is shown to be complementary to classical nucleation theory.

This insight was enabled through exploitation of the supersaturation rate which can directly relate mass and heat transfer processes within the boundary layer to nucleation theory. The modified power law relation demonstrates that nucleation rate is driven by the interfacial supersaturation, the extent of change being dependent on the crystal-liquid interfacial energy of the salt. Consequently, T and ΔT can be collectively used to set supersaturation level within the boundary layer to control the final crystal product properties. The capability to relate complex simultaneous mass and heat transfer processes in the boundary layer to nucleation control is unique to membrane processes. This provides simplification for technology scale-up which is otherwise a major challenge to conventional crystalliser design. The supersaturation level at the intersection between heterogeneous and homogeneous primary nucleation mechanisms is specific to kinetically controlled scale formation. This value can be adopted generically as a critical threshold to ‘switch-off’ scaling by NaCl. However, a rapid flux decline is still observed in the absence of scaling due to the subsequent deposition of crystals from the bulk solution. Further work is therefore required to better understand the mechanistic principles governing the backtransport of solid particles in membrane distillation as a method to advance more sustainable operation.

CRedit authorship contribution statement

A. Mapetere: Writing – original draft, Methodology, Investigation, Formal analysis, Data curation, Conceptualization. **G. Di Profio:** Writing – review & editing, Formal analysis. **E. Curcio:** Writing – review & editing, Formal analysis. **P. Campo:** Writing – review & editing, Supervision, Methodology, Formal analysis, Conceptualization. **E.J. McAdam:** Writing – review & editing, Supervision, Project administration, Methodology, Funding acquisition, Formal analysis, Data curation, Conceptualization.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Data availability

The data underlying this paper can be accessed through the following link: <https://doi.org/10.57996/cran.ceres-2747>.

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Unifying nucleation and crystal growth mechanisms in membrane crystallisation

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